

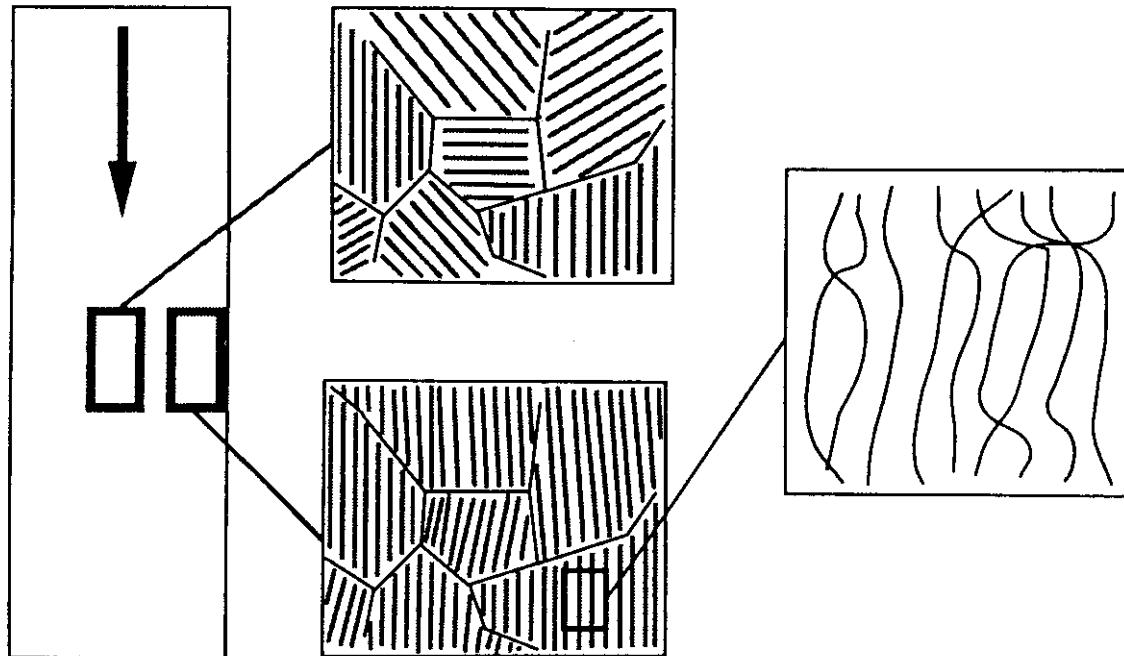
Chapter 9. Chain orientation

9.1 Introduction

Anisotropic property of polymer :

strong covalent bonds along the chain axis

weak secondary bonds in the transverse directions



9.2 Definition of chain orientation

Average end-to-end distance

$$\langle r \rangle_0 = C \sqrt{n} l$$

C : constant depending on the segmental flexibility

l : bond length

n : number of bonds

Fully oriented molecule, $r_\infty = nl$

∴ Strain to reach the completely aligned state

$$\lambda = \frac{r_\infty}{\langle r \rangle_0} = \frac{\sqrt{n}}{C} \Rightarrow \lambda \uparrow \text{ with } \sqrt{M}$$

* **Hermans orientation function, f**

Polarizability :

$$p_{zz} = p_1 \cos^2 \phi + p_2 \sin^2 \phi$$

$$p_{xx} = p_2 + (p_1 - p_2) \sin^2 \phi \cos^2 \nu$$

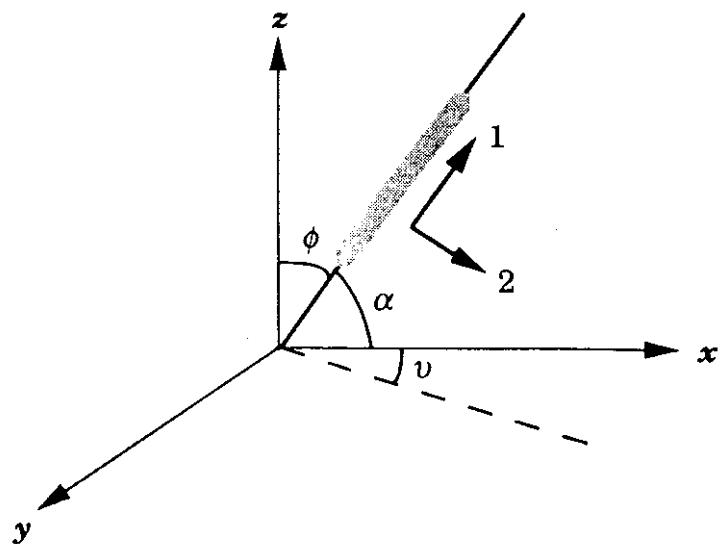


Figure 9.4 Chain segment and coordinate system.

Lorentz-Lorenz equation :

$$\frac{n_{ij}^2 - 1}{n_{ij}^2 + 2} = \frac{4\pi}{3} p_{ij}$$

p_{ij} can be converted to n_{ij}

p_{ij} : polarizability tensor

n_{ij} : refractive index tensor

Birefringence (Δn) : $\Delta n = n_{zz} - n_{xx}$

Average refractive index $\langle n \rangle$, $\langle n \rangle = \frac{1}{2}(n_{xx} + n_{zz})$

$$\Rightarrow \dots \Rightarrow \Delta n = \frac{(\langle n \rangle^2 - 2)^2}{6\langle n \rangle} \frac{4\pi}{3} (p_1 - p_2) \left(1 - \frac{3\langle \sin^2 \phi \rangle}{2} \right)$$

Hermans orientation function :

$$f = \frac{\Delta n}{\Delta n_0} = \frac{3\langle \cos^2 \phi \rangle - 1}{2} \quad \leftarrow \text{for 3-dimensional}$$

$$= 2\langle \cos^2 \phi \rangle - 1 \quad \leftarrow \text{for 2-dimensional}$$

$$= \frac{2}{n} \sum_{i=1}^n \cos^2 \phi_i - 1$$

Δn_0 : maximum birefringence

※ For 3-dimensional orientation,

$f = 1$ (parallel), -0.5 (perpendicular), 0 (random) → Fig. 9.5

For 2-dimensional orientation,

$f = 1$ (parallel), -1 (perpendicular), 0 (random)

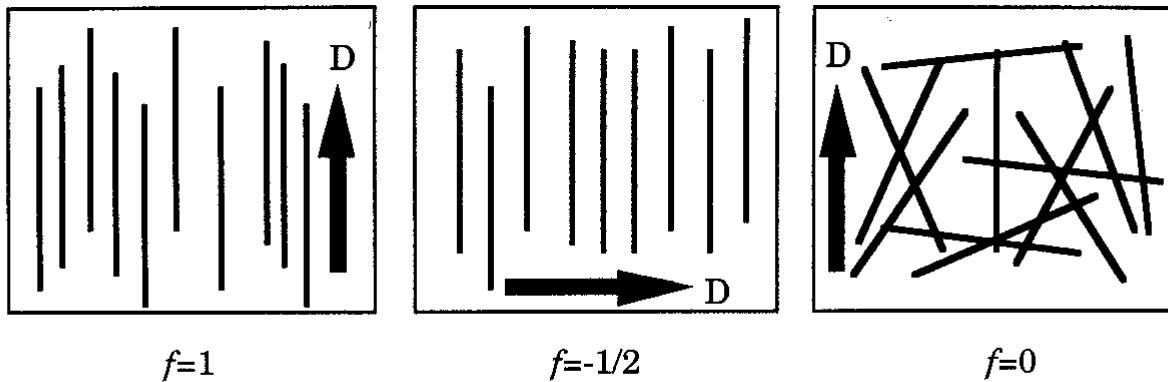
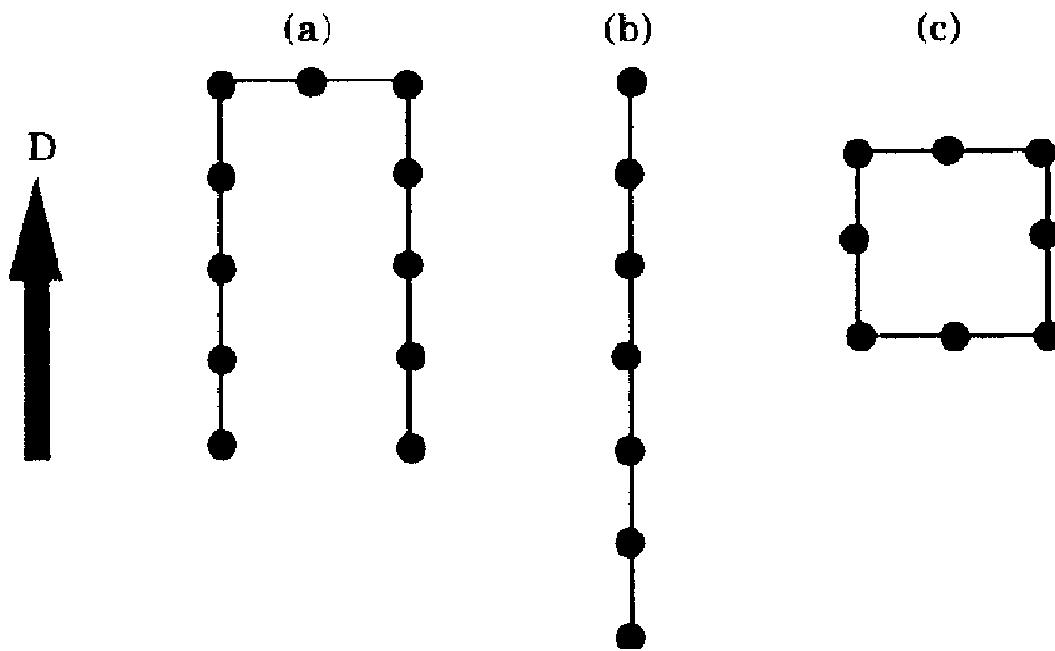


Figure 9.5 Values for the Hermans orientation function for three simple cases. The director (D) is shown for each case.

Ex)



two-dimensional orientation, (a) $f = 0.6$, (b) $f = 1$, (c) $f = 0$

* **Birefringence**

$$\Delta n = \Delta n_f + \Delta n_d + \Delta n_c + \Delta n_a$$

where, Δn_f : form birefringence (occurs only in multiphase systems)

Δn_d : deformation birefringence (may cause stresses in bonds)

$\Delta n_c + \Delta n_a$: orientation-induced birefringence (originating from
the crystalline and the amorphous components)

If orientation is uniaxial & both form and deformation birefringence
can be neglected,

$$\Delta n = \Delta n_c + \Delta n_a = \Delta n_0 [w_c f_c + (1 - w_c) f_a]$$

w_c : crystallinity

f_c, f_a : f of crystalline and amorphous components

Birefringence measurements

⇒ " *polarized light microscope* "

Compensator

-- optical retardation (R_{31})

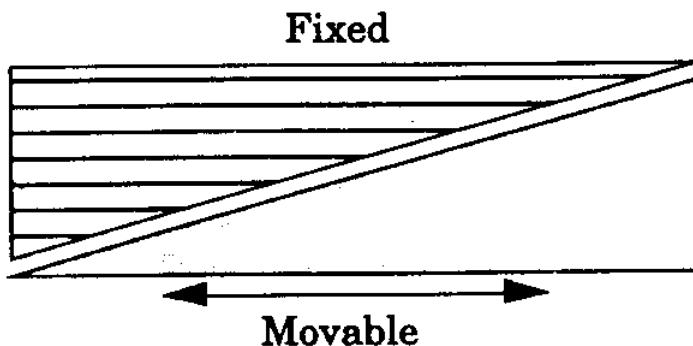


Figure 9.8 Babinet compensator which consists of two quartz wedges with crossed optical axes.

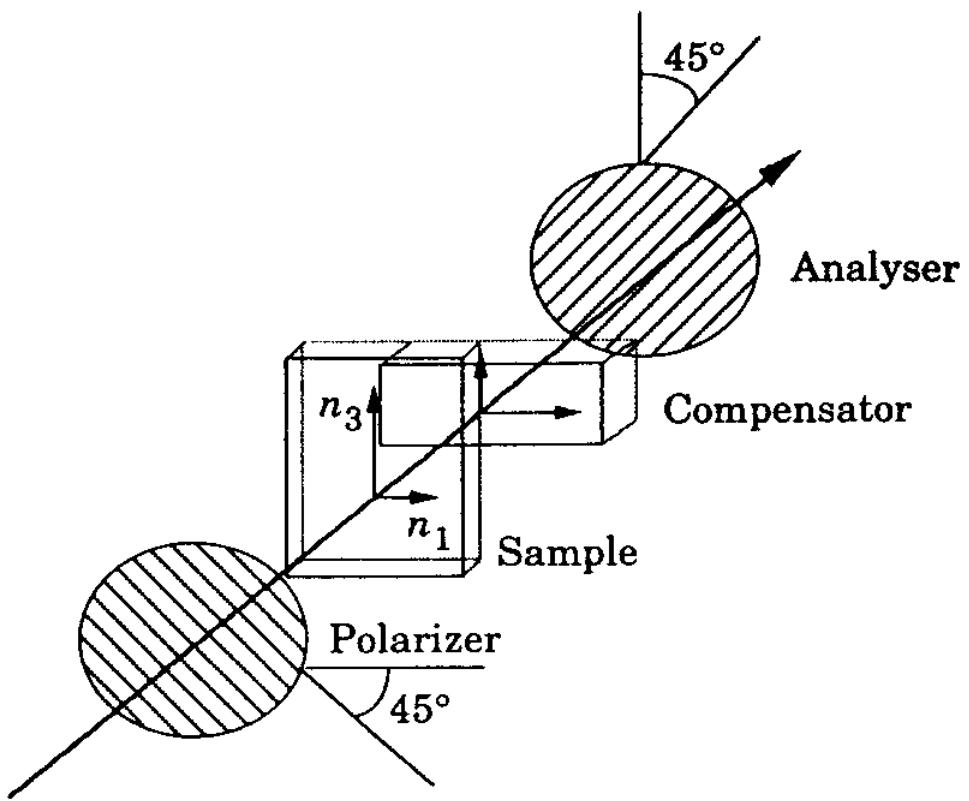


Figure 9.9 Optical system for the measurement of orientation in the plane.

In-plane birefringence ($\Delta n = n_3 - n_1$),

$$\Delta n = \frac{R_{31}\lambda}{d}$$

λ : wavelength of the light

d : sample thickness

Thinner sample (< 100 μm) can be measured by white light source

(visible light : wavelength from 400 nm (violet) to 750 nm (red))

← semicrystalline polymers

Clear amorphous polymers → thick sample도 가능

Color as a function of optical retardation ⇒ "Michel-Levy chart"

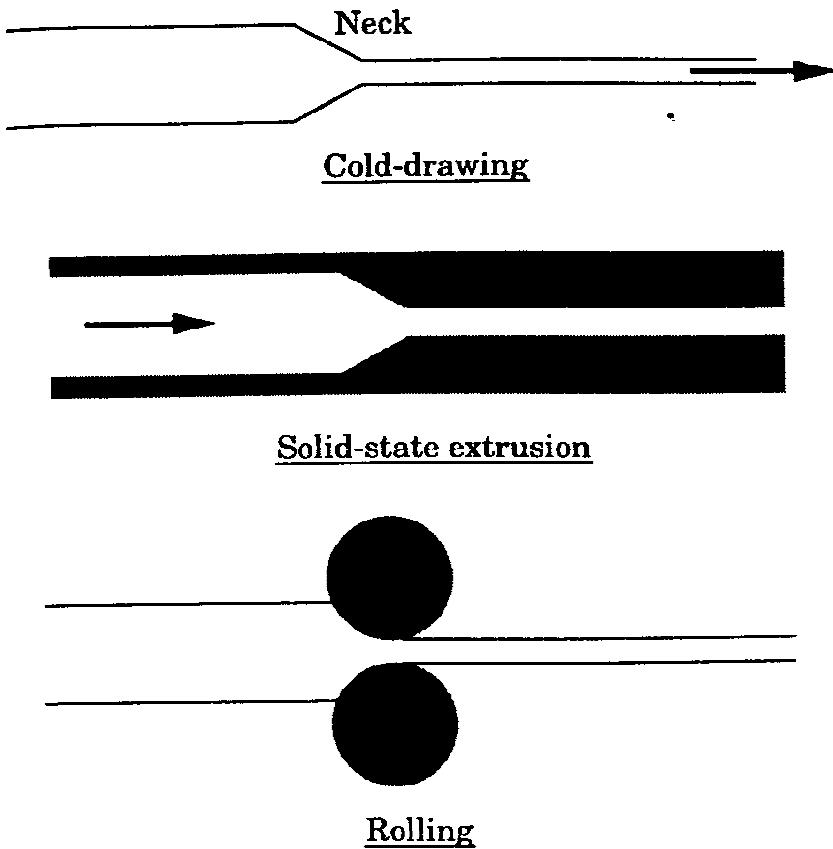
보다 두꺼운 sample (ex, mm 두께의 PE) – far infrared interferometry로 관찰

9.5 Chain orientation by processing

* Solid-state processes

- Cold-drawing
- Solid-state extrusion
- Rolling

$$\lambda = \frac{L}{L_0} \approx \frac{A_0}{A} : \text{draw ratio}$$



For semicrystalline polymers,

- deformation of spherulite structure
- spherulite → fibrillar structure
- plastic deformation of the fibrillar structure

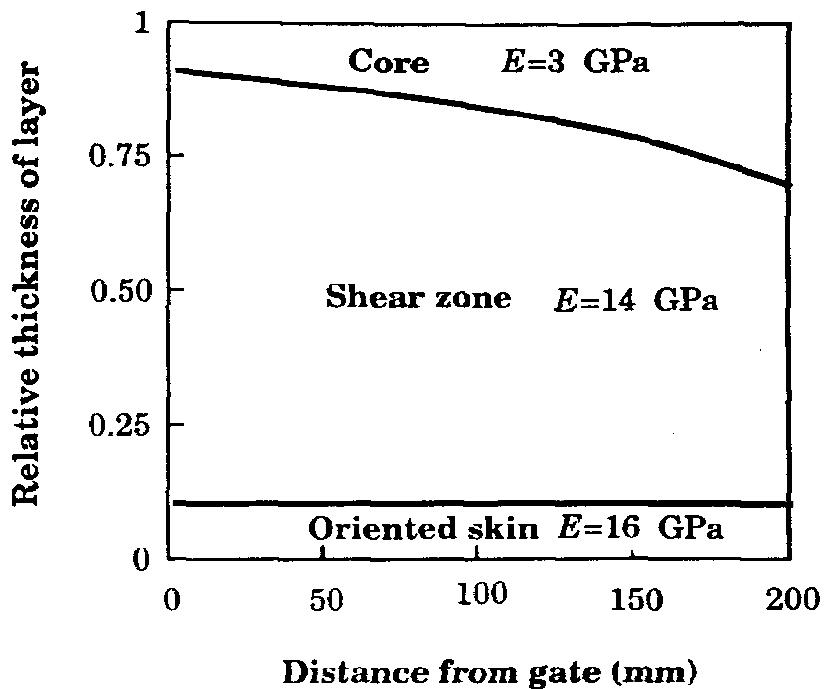
Crystal thickness (L_c) of the fibrous polymer

$$L_c = \frac{C_1}{\Delta T} + C_2$$

ΔT : degree of supercooling

* Liquid processes

- molding (Fig. 9.19 : microstructural layer of a 3 mm thick injection molded ruler)
- spinning (melt-spinning, solution-spinning), etc.



" shear flow "

&

" elongational flow "

=> Relative thickness of microstructural layers of a 3mm thick injection-molded ruler of a liquid-crystalline polymer

9.6 Properties of oriented polymers

Axial elastic modulus for a few polymers

Table 9.1 The maximum elastic modulus at room temperature of a few selected polymers

Polymer	Elastic modulus (GPa)
Polyethylene	240–360
Isotactic polypropylene	42
Polyoxymethylene	54
Poly(ethylene terephthalate)	140
Polyamide 6	250
Diamond	800

Elastic deformation (comparative values) of a single molecule occurs by

- bond stretching 100
- bond-angle deformation 10
- torsion about a σ bond 1

ex.)

Diamond : 3-dimensional covalent-bond structure \leftarrow stretching

PE, PA6 : all-trans form (fully-extended) \leftarrow stretching and deformation

IPP, POM : helical conformations \leftarrow stretching, deformation and torsion

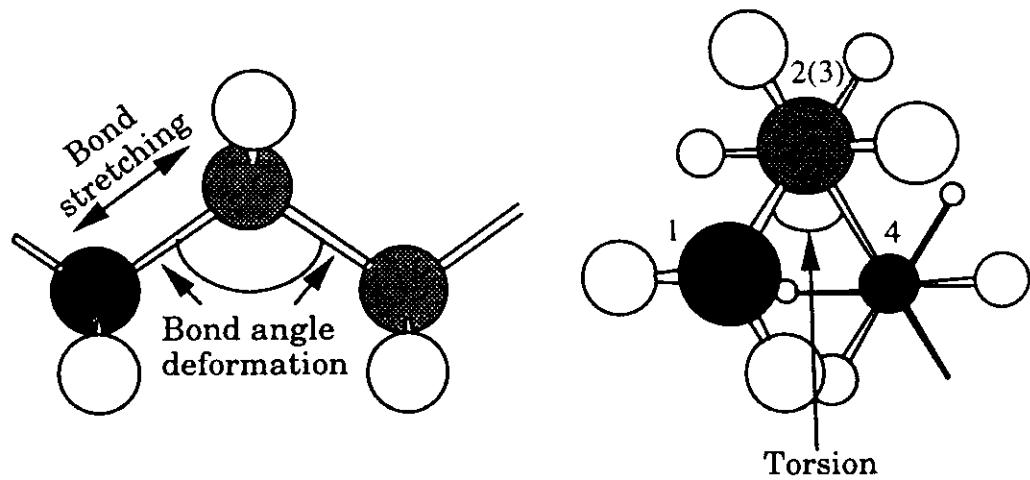


Figure 9.20 Deformation of a polyethylene molecule by bond stretching, bond angle deformation (both left-hand side) and torsion about the σ bond linking carbons 2 and 3 (right-hand side).

Table 9.2 Summary of relationships between chain orientation and a few selected properties

Property	Relation	Other relations
Birefringence (Δn)	$\Delta n = \Delta n_0 f$ Uniaxial orientation ^a	$n_3 - n_1 = \Delta n_0 \left(f - \frac{g}{2} \right)$ $n_3 - n_2 = \Delta n_0 \left(f + \frac{g}{2} \right)$ $n_1 - n_2 = \Delta n_0 g$ Biaxial orientation ^b
Thermal expansivity (α)	Linear expansivities: ^c $\alpha_{\parallel} = \alpha_0 - \frac{2}{3}(\alpha_2 - \alpha_1)f$ $\alpha_{\perp} = \alpha_0 + \frac{1}{3}(\alpha_2 - \alpha_1)f$ Uniaxial orientation	Volume expansivity: $\alpha_v = \alpha_{\parallel} + 2\alpha_{\perp} = \text{const.}$
Thermal conductivity (λ_c)	$\frac{1}{\lambda_{c\parallel}} = \frac{1}{\lambda_{c0}} - \frac{2}{3} \left(\frac{\frac{1}{\lambda_{c2}} - \frac{1}{\lambda_{c1}}}{f} \right)$ Uniaxial orientation ^d	$\frac{1}{\lambda_{c\perp}} = \frac{1}{\lambda_{c0}} + \frac{1}{3} \left(\frac{\frac{1}{\lambda_{c2}} - \frac{1}{\lambda_{c1}}}{f} \right)$ Uniaxial orientation
Elastic compliance (J)	$\frac{J_{\parallel}}{J_0} = 1 - f$ Uniaxial orientation simplified formula; small/medium f values	For ultra-oriented polymers: good correlation only with draw ratio