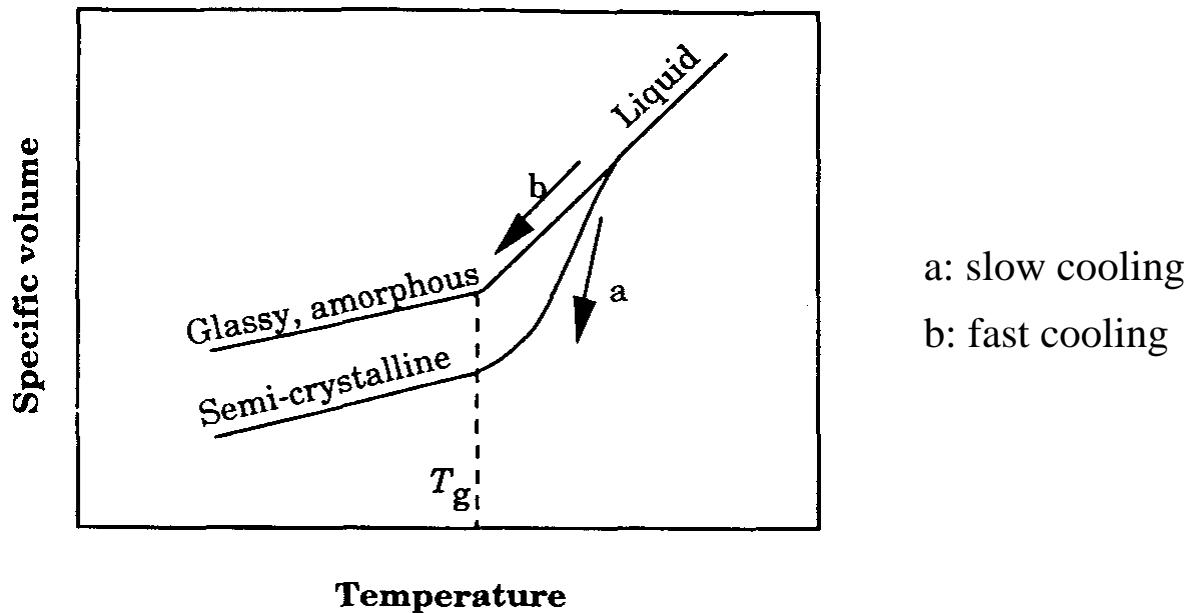


# Chapter 5. Glassy Amorphous State

## 5.1 Introduction

Molten polymer --> (cooling) --> glassy, amorphous  
semi-crystalline



a: slow cooling

b: fast cooling

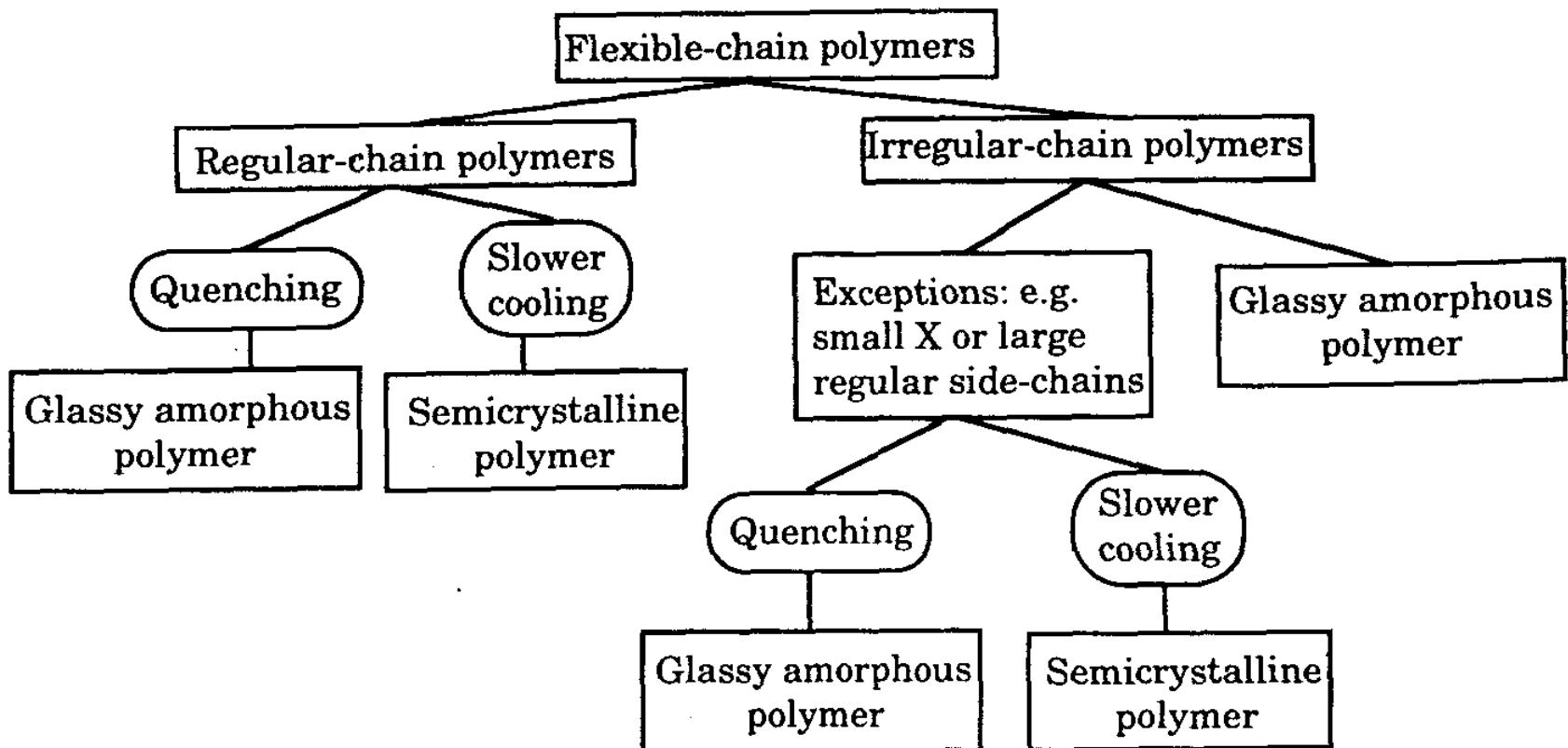
- *Key factor* of crystallizing a polymer : regularity of the polymer

Atactic polymers : do not crystallize

ex) IPP : crystallize

atactic PP : not

Exceptions) 1. X group in  $\text{---}(\text{CH}_2\text{CHX})_n\text{---}$  is very small. ex.) PVAL  
2. X group of a long regular side chain (side chain crystallization)



Effect of molecular and thermal factors of the structure of solidified polymer  
 $\therefore T_g$  values depend on experimental conditions.

## 5.2 Glass transition temperature

\* Effect of repeating unit structure



- relatively inflexible X group:  $T_g \uparrow$  with size of the group  $\uparrow$

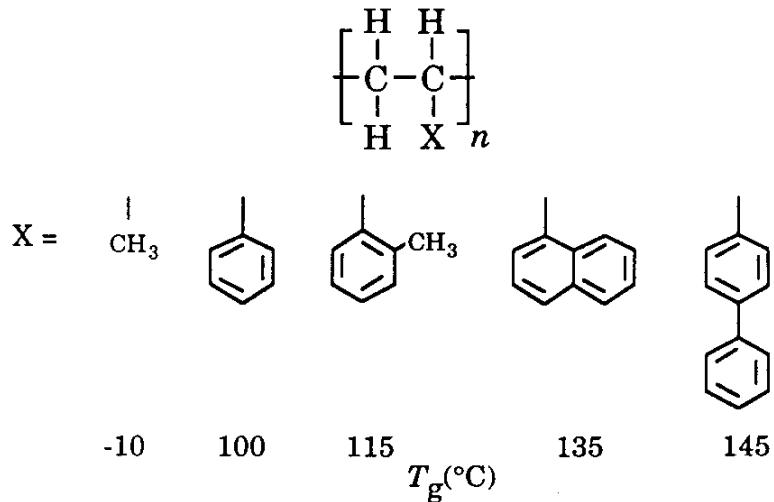
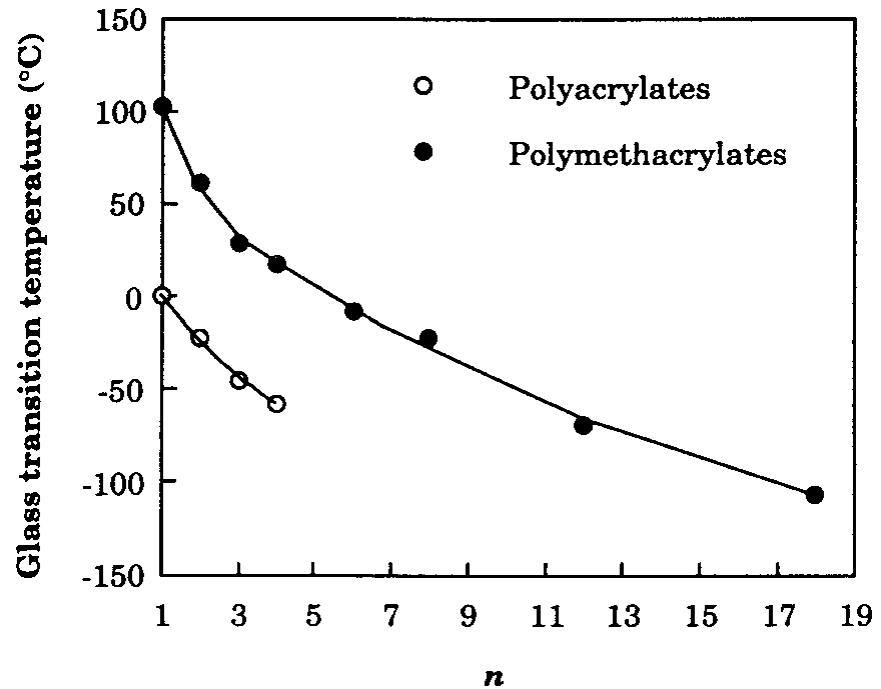


Figure 5.3 Glass transition temperatures of different vinyl polymers showing the influence of the size of the pendant group. Data from Eisenberger (1984).

- relatively flexible side chain :  $T_g \downarrow$  with length of the side chain  $\uparrow$



$n$  : the number of carbons in  
the oligo-methylene (R)  
group

- longer pendant groups  $\rightarrow T_g \uparrow$

- $T_g \uparrow$  with increasing *polarity* ( $T_g \uparrow$  with Cl content  $\uparrow$ ), C-Cl : polar

→ generally,  $T_g = \frac{2\delta^2}{mR} + C_1$

$\delta^2$  : CED (cohesive energy density)

m : internal mobility of the groups in a single chain

$T_g$  &  $T_m \uparrow$  with chain flexibility  $\downarrow$

$T_g$  &  $T_m \uparrow$  with CED  $\uparrow$

$$\frac{T_g}{T_m} = \frac{1}{2} \quad (\text{symmetrical molecules})$$

$$\frac{T_g}{T_m} = \frac{2}{3} \quad (\text{asymmetrical molecules})$$

$$\frac{T_g}{T_m} = 0.5 \sim 0.8$$

### \* Free volume

volume { free volume  
                occupied volume

$$f(\text{fractional free volume}) = \frac{\text{free volume}}{\text{total volume}}$$

Ideal crystal :  $f \simeq 0$

Glassy, amorphous polymer : relatively small  $f$

Amorphous, rubber polymer : relatively large  $f$

Estimation of the size of empty volume  $\Rightarrow$  X-ray scattering

\* **Effect of molecular architecture** on  $T_g$

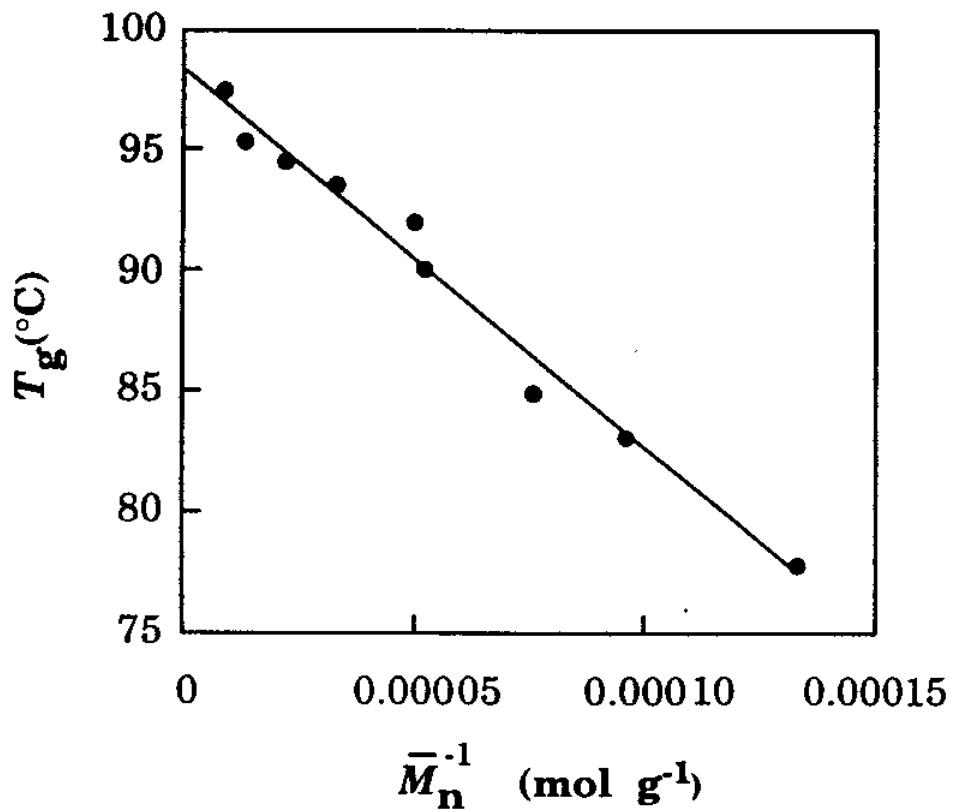
: Molar mass, degree of crosslinking, chain branching

$$\cdot f = f^0 + \frac{C_2}{M} \quad f^0 \rightarrow f \text{ of the polymer of infinite molar mass}$$

$$\approx (C_3 + C_4 T) + \frac{C_2}{M} \quad (\text{temperature dependence})$$

$$\Rightarrow T_g \approx \frac{f_g - C_3}{C_4} - \frac{C_2}{C_4 M} = C_5 - \frac{C_6}{M}$$

$f_g$  : (universal fractional free volume)  $\rightarrow$  fractional free volume at  $T_g$



Dependence of  $T_g$  on molar mass for narrow fractions of atactic polystyrene

- Crosslinks reduce  $f$

$$f \approx f^0 - n_c C_7 = f^0 - \frac{C_8}{\overline{M}_c}$$

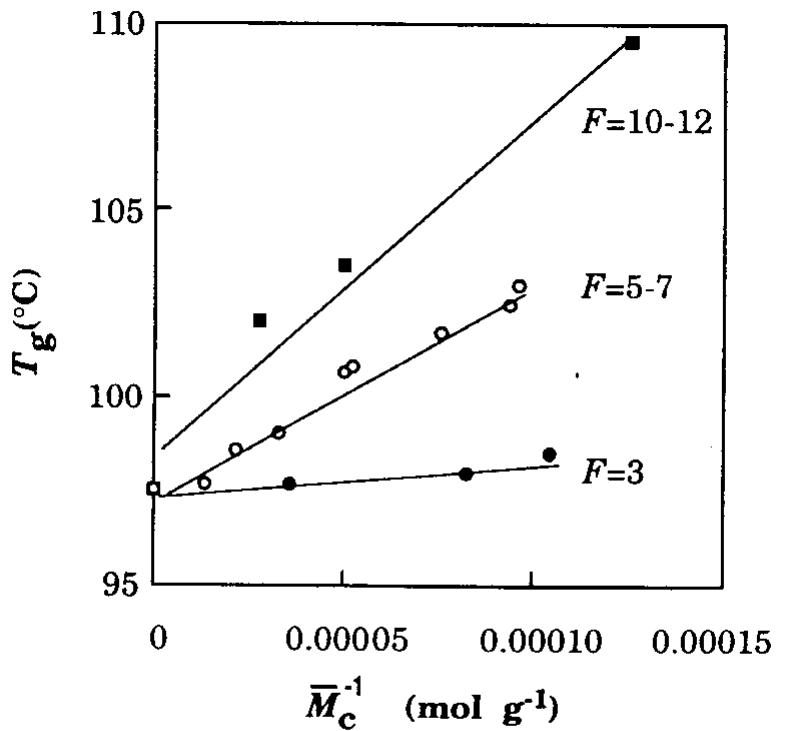
$n_c$  : # of crosslinks

$\overline{M}_c$  : number average MW of the chains between crosslinks

$$T_g \approx C_9 + \frac{C_{10}}{\overline{M}_c} \text{ by analogy with } M \text{ dependence}$$

In a polymer of  $M$  &  $\overline{M}_c$ ,

$$T_g \approx C - \frac{C'}{M} + \frac{C''}{\overline{M}_c}$$

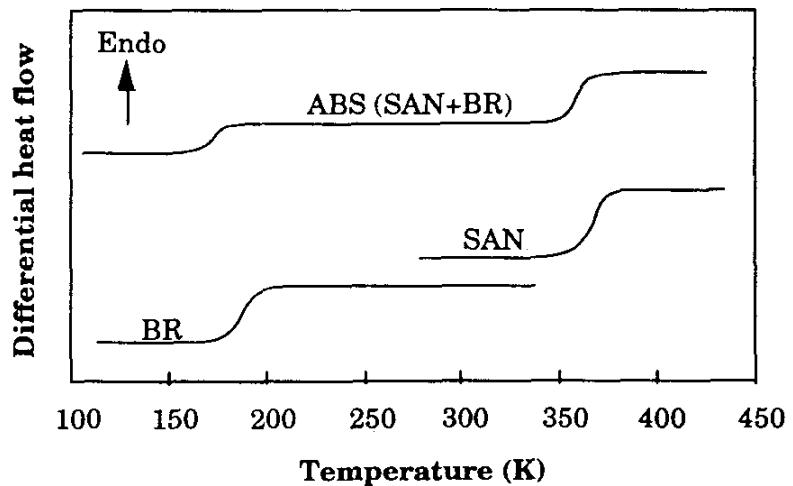


**Figure 5.9** Effect of crosslinking on  $T_g$  of branched poly(styrene-*co*-divinyl benzene). The crosslink functionality ( $F$ ) is shown adjacent to each regression line. Drawn after data from Rietsch, Daveloose and Froelich (1976).

\*  $T_g$  of **blends & copolymers**

: highly dependent on the morphology

Immiscible polymer blend → two  $T_g$ 's



**Figure 5.10** DSC traces of ABS and of its constituents poly(butadiene) (BR) and poly(styrene-co-acrylonitrile) (SAN). Schematic after data from Bair (1970).

Miscible polymer blend  $\rightarrow$  one  $T_g$

: Fox equation,

$$\frac{1}{T_g} = \frac{w_1}{T_{g1}} + \frac{w_2}{T_{g2}}$$

$\Downarrow$

$$\frac{1}{T_g} = \sum \frac{w_i}{T_{gi}}$$

$w_i$  : wt. fraction of polymer  $i$

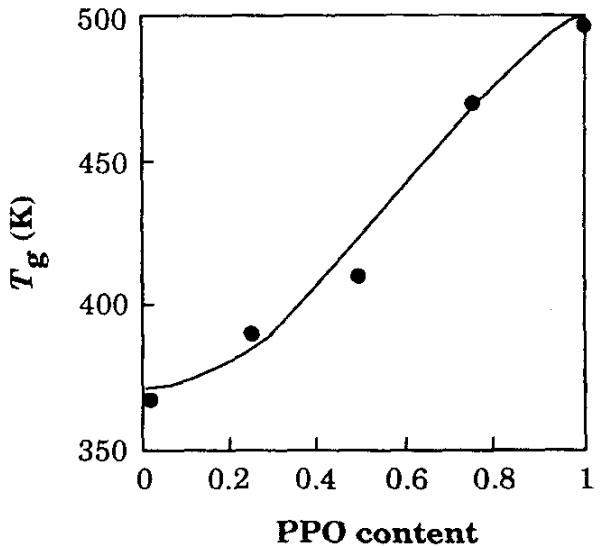
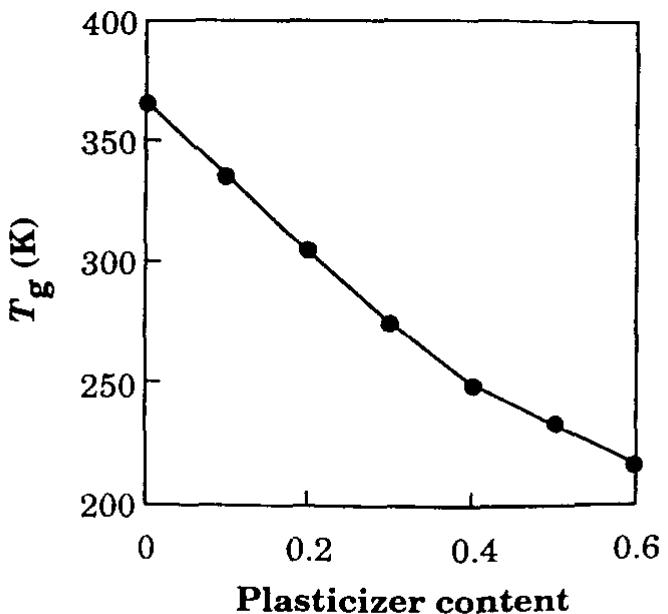


Figure 5.11 Glass transition temperature of compatible blends of polystyrene and polyphenylene oxide (PPO) as a function of PPO content. Drawn after data from Bair (1970).



**Figure 5.12** Plasticization of PVC:  $T_g$  as a function of di(ethylhexyl)-phthalate content. Drawn after data from Wolf (1951).

Plasticizer : low MW liquid having a strong  $T_g$ -depressive effect

\* **P effect** on  $T_g$

$$\left( \frac{dT_g}{dp} \right) = \frac{\Delta\beta}{\Delta\alpha}$$

$\alpha$ : volume expansion coefficient

$$\equiv \frac{1}{V} \left( \frac{dV}{dT} \right)_p$$

$\beta$ : compressibility coefficient

$$\equiv -\frac{1}{V} \left( \frac{dV}{dp} \right)_T$$

Typical polymers : 0.2 ~ 0.4K/MPa

## 5.3 Non-equilibrium feature

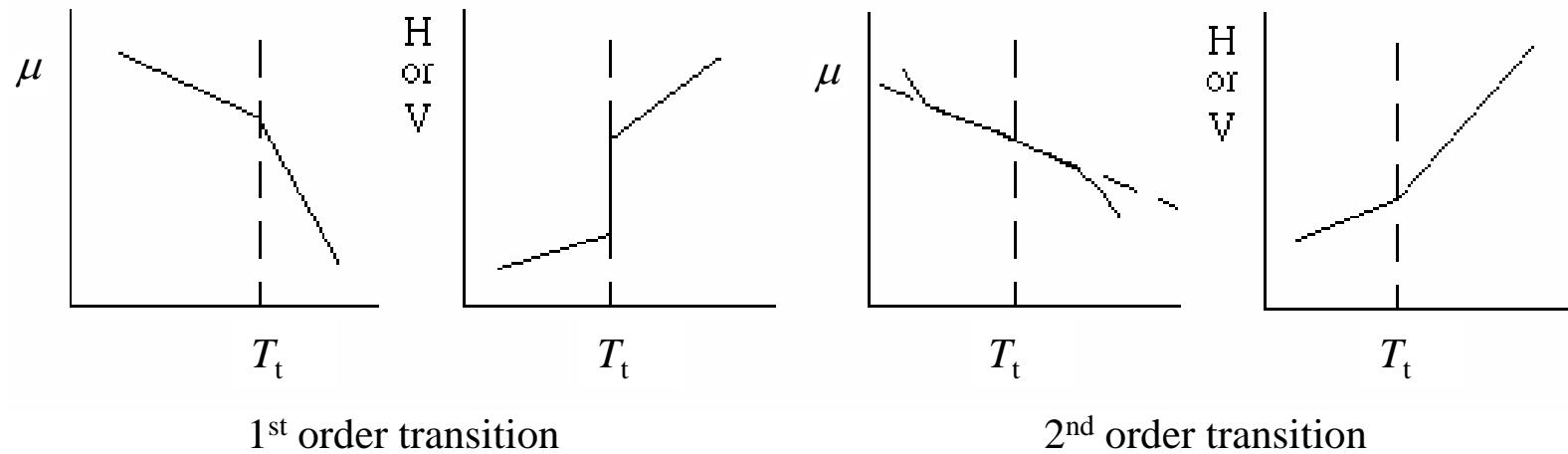
### \* General aspects

glass transition : second-order transition

정의 :  $\mu$  의  $T$ 에 대한 2계 미분이 discontinuous.

The 1st derivatives of  $V$  &  $H$  w.r.t.  $T$  are discontinuous.

cf.)  $\mu$  의 1계 미분이 불연속  $\rightarrow$  1st-order transition ( $V, H$  자체가 불연속)



\* **Non-equilibrium nature** of a glassy polymer

At constant cooling rate,  $q$

Point B : kinetic glass transition.

$V$  decreases under isothermal condition ( $C \rightarrow D$ )

“physical ageing”

or

“isothermal volume recovery”

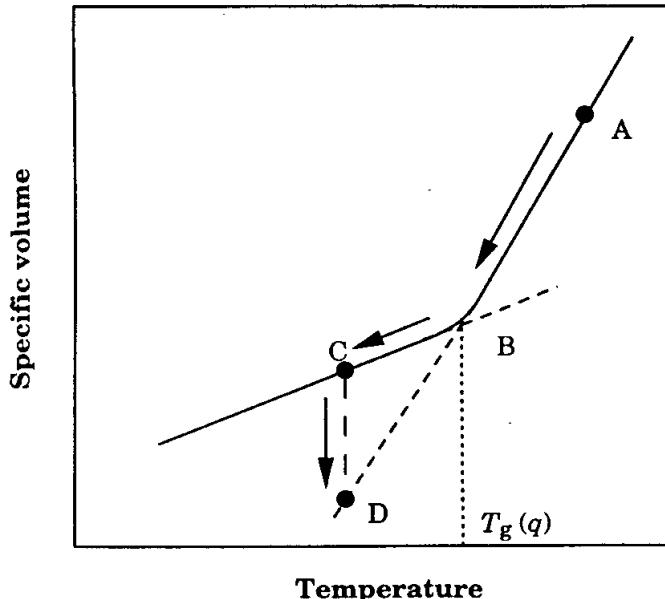


Figure 5.13 Illustration of the non-equilibrium nature of a glassy polymer.

\* **Volumetric response** to different cooling rates (See Fig. 5.14)

$T_g$  changes : 3K for a change by a factor of 10 in cooling rate.

- Volume recovery

→ Contraction is more rapid than expansion.

An amorphous polymer which is cooled rapidly through  $T_g$  and then held at const.  $T$

⇒  $V \& H \downarrow$ ,  $G$  (tensile modulus)  $\uparrow$ ,  
 $\sigma_0$  (yield stress)  $\uparrow$ , toughness  $\downarrow$ ,  
impact strength  $\downarrow$ , permeability  $\downarrow$

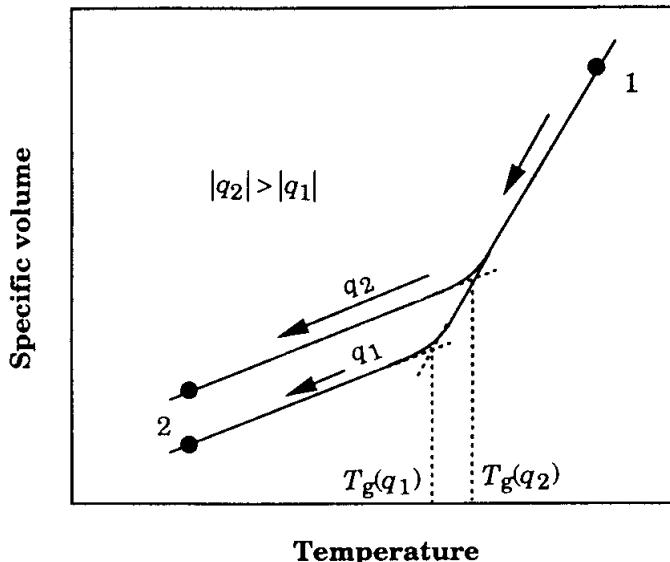


Figure 5.14 Schematic curves showing the cooling rate dependence of the specific volume of a glass-forming wholly amorphous polymer.