

# Chapter 9 Mixing and Segregation

## 9.1 Introduction

☞ [http://sol.rutgers.edu/~shinbrot/Group\\_Index.html](http://sol.rutgers.edu/~shinbrot/Group_Index.html)

## 9.2 Types of Mixture

\* *Perfect mixing*

*Random mixing*

*Segregating mixing*

Figure 9.1

## 9.3 Segregation

### (1) Causes and Consequences of Segregation

- The phenomena by which the particles with *the same* physical property (size, density and shape) *collect together* in one part of the mixture. Among them *particle size* is *most important* cause for segregation mechanisms
- Usually it occurs during *moving, pouring, conveying, processing*
- Its degree depends on *particle-particle interaction\**

\* *Free-flowing powder* or *coarse particles* → *segregating* rather than  
mixing

*Cohesive powder* or *fine particles* → mixing rather than  
segregating but easily  
*aggregating*

### (2) Mechanisms of Separation Figure 9-2

- *Trajectory segregation*

From Chapter 3 in lecture note,

Stop distance  $s = \tau U = \frac{\rho_p d_p^2 U}{18\mu}$ , 큰 입자가 멀리 간다.

- *Percolation* of fine particles - Figure 9.3

작은 입자가 큰입자의 사이를 파고 들고 큰입자가 걸, 작은 입자가 속을 차지한다.

Rise of coarse particles on vibration - Figure 9.4

- *Elutriation* segregation

기체는 침강속도가 작은 입자를 들어올리나 침강속도가 큰 입자는 그대로 내려 오게 한다.

### (3) Reduction of Segregation

Make the *sizes* of the components as *close* as possible

Reduce the *absolute size* of the particles

(< 30  $\mu m$  with density about  $\rho_p = 2000-3000 \text{kg/m}^3$ )

- Use of interparticulate forces

- Critical diameter lowered as the density increases.

Add a small amount of *liquid*.

- Use of liquid-bridge force

Make *one of the components very fine* (less than 5  $\mu m$ )

- *Ordered mixing\**

Figure 9.5

Avoid to promote the segregation

e.g. use mass flow instead of core flow

Use continuous mixing for very segregating materials

## 9.5 Equipment for Particulate Mixing

### (1) Mechanisms of Mixing

*Diffusive mixing*: random walk phenomenon

- Essential for microscopic homogenization

- Not suitable for segregating particles

e.g. Tumbling mixers : Figure 9.6

*Shear mixing*: induced by the momentum exchange of powders having  
different velocities

- Semimicroscopic mixing

e.g. High-velocity rotating blade

Low velocity-high compression rollers

☞ Chapter 10

*Convective mixing*: circulation of powders

- Beneficial for batch mode, not for continuous mixing

- Suitable for segregating particles

e.g. Ribbon blender : Figures 9.7, 9.8

Fluidized-bed mixer

Effect of particle size on mixing patterns

## (2) Types of Mixers

*Tumbling mixers*, Figure 9.6

- Closed vessel rotating about axis
- dominant in *diffusive* mixing
- makes segregation for free flowing particles
- baffle installed has little effect

*Convective mixers*, Figures 9.7, 9.8

- static shell by *rotating blades or paddles*, < 1rps
- accompanied by some diffusive and shear mixing

*Fluidized mixers*

- largely *convective* by bubble motion
- mixing, reaction coating, drying etc. : carried out in the same vessel

*High shear mixers*

- high shear created by high velocity rotating blades

low velocity-high compression rollers

- breaking down agglomerates of cohesive powders

\* *Ordered mixture*

- Dry impact blending method
- Mechanofusion method

**(3) Power Requirement for Mixing**

$$P = 2\pi N_s T$$

where  $N_s$ : rotation speed(rps)

$T$  ?

- Horizontal Cylinder Mixer

$$\frac{T}{R^3 L \rho_b g} = A + B \frac{N_s^2 R}{g}$$

where  $R$  : radius of rotation

$A$  and  $B$  : depend on powder properties

- V-Type Mixer

$$\frac{T_j}{R_{\max}^4 \rho_b g} = A_j + B_j \frac{N_s^2 R_{\max}}{g}$$

where  $A$  and  $B$  : depend on powder properties

- Stationary Vessel Mixer-ribbon and paddle impeller

$$T = K d_p^{a_1} \rho_b^{a_2} \mu_s^{a_3} Z^{a_4} D^{a_5} \left( \frac{S}{D} \right)^{a_6} b^{a_7} f^{a_8}, \quad (\text{N} \cdot \text{m})$$

where  $d_p$ : particle diameter(m)

$\rho_b$ : bulk density(kg/m<sup>3</sup>)

$\mu_0$ : internal friction coefficient

$S$ : pitch of ribbon impeller(m)

$b$ : width of impeller(m)

$D$ : diameter of impeller(m)

$f$ : charge ratio

$Z$ : height of powder bed(m)

$K, \alpha_i$ 's: depend on the type of mixers

## 9.6 Assessing the Mixture

For Binary mixture(2 components)

If  $y_i(i=1,2,\dots,N)$ : composition of the key component in the  $i$ -th sample,

*Sample mean*

$$\bar{y} = \frac{1}{N} \sum_{i=1}^N y_i$$

*True mean*

$$\mu = \bar{y} \pm \frac{tS}{\sqrt{N}}$$

where  $t$  : percentile value for *student's t distribution*

☞ *Shaum's-Mathematical handbook*

depends on *the level of confidence and the number of freedom(N)*

e.g. for 97.5% confidence and  $N=60$

$$t = 2.00$$

$S$  : the *estimated standard deviation*

Standard deviation,  $\sigma$  and standard variance,  $\sigma^2$

- *Estimated standard variance* ( $S^2$ )

$$S^2 = \frac{1}{N} \sum_{i=1}^N (y_i - \mu)^2$$

if true mean is known, otherwise

$$S^2 = \frac{1}{N} \sum_{i=1}^N (y_i - \bar{y})^2$$

- *Theoretical Limits of variance*

Upper limit: true standard deviation for a completely unmixed system,  $\sigma_0$

$$\sigma_0^2 = p(1-p)$$

Lower limit: true standard deviation of random binary mixture,  $\sigma_r$

$$\sigma_R^2 = \frac{p(1-p)}{n}$$

where  $p, 1-p$  : fractions of two components in the whole mixture

- True variance,  $\sigma$

when  $N > 50$

$$\sigma^2 = S^2 \pm [t \times E(S^2)]$$

$$\text{where } E(S^2) = S^2 \sqrt{\frac{2}{N}}$$

When  $N < 50$

$$\text{Lower limit: } \sigma_L = \frac{S^2(N-1)}{X_{\alpha}^2}$$

$$\text{Upper limit: } \sigma_U = \frac{S^2(N-1)}{X_{1-\alpha}^2}$$

where  $X_{\alpha}$ : *chi-squared distribution* for significance level,  $\alpha$

$\alpha = 0.5(1-c)$  where  $c$ : confidence range

e.g.  $c = 0.9 \rightarrow \alpha = 0.05 \rightarrow X_{0.05}^2 = 34.8$  for  $N = 50$

- Degree of Mixing (Mixing indices)

the ratio of mixing achieved to mixing possible

$$\text{Lacey : } \frac{\sigma_0^2 - \sigma^2}{\sigma_0^2 - \sigma_r^2}$$

$$\text{Poole : } \frac{\sigma}{\sigma_r}$$

Worked Example 9.1, 9.2, 9.3