

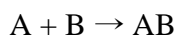
## CHME 312, Reaction Engineering, 2011 Spring

### Exam III, Open Text (H. Scott Fogler, *Elements of Chemical Reaction Engineering*)

**Note: For partial credit, please write your answer clearly and legibly.**

**For better credit, do all algebra and substitute digits, and check final figures carefully.**

1. An irreversible reaction was studied to find out its kinetics.



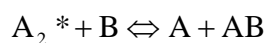
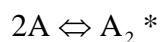
They found the production rate was expressed as  $r_{AB} = kC_B^2$ , almost independent of the  $C_A$ . Assuming that intermediates consist of association of reactants and the reaction has no chain reaction, suggest the **reaction mechanism** including such conditions which satisfy the expression found. (50)

Sol)

- If this reaction is elementary, then  $r_{AB} = kC_A C_B$  the result is different from this assumption.

- Let's try with some non-elementary mechanisms

1) Assuming 2 step reactions with intermediate  $A_2^*$



This reactions can be rearrange to give 4 elementary reactions



- The production rate of AB is, by equation (3) and (4)

$$r_{AB} = k_3 C_{A_2^*} C_B - k_4 C_A C_{AB} \quad (5)$$

- Since  $C_{A_2^*}$  is extremely small and we cannot measure it, we need to express  $C_{A_2^*}$  in terms of measurable quantities,  $C_A$ ,  $C_B$ , or  $C_{AB}$ .

$$r_{A_2^*} = \frac{1}{2}k_1C_A^2 - k_2C_{A_2^*} - k_3C_{A_2^*}C_B + k_4C_A C_{AB}$$

- $C_{A_2^*}$  is very small and  $r_{A_2^*}$  is considered as 0  $\Rightarrow$  PSSH

$$C_{A_2^*} = \frac{\frac{1}{2}k_1C_A^2 + k_4C_A C_{AB}}{k_2 + k_3C_B}$$

$$r_{AB} = \frac{\frac{1}{2}k_1k_3C_A^2C_B - k_2k_4C_A C_{AB}}{k_2 + k_3C_B} \quad (6)$$

- If  $k_2$  is very small, equation (6) can be simplified as

$$r_{AB} = \frac{1}{2}k_1C_A^2 \quad (7)$$

$\Rightarrow$  This is a symmetry case of A with B observed.

- If  $k_4$  is very small, equation (6) can be simplified as

$$r_{AB} = \frac{(k_1k_3/2k_2)C_A^2C_B}{1 + (k_3/k_2)C_B} \quad \Rightarrow \text{If } C_B \text{ is small it can be expressed as } r_{AB} = \frac{k_1k_3}{2k_2}C_A^2$$

$\Rightarrow$  This is a symmetry case of A with B observed.

- 2) Assuming 2 step reactions with intermediate  $B_2^*$



- The production rate of AB is, by equation (3) and (4)

$$r_{AB} = k_3C_{B_2^*}C_A - k_4C_B C_{AB} \quad (5)$$

- Since  $C_{B_2^*}$  is extremely small and we cannot measure it, we need to express  $C_{B_2^*}$  in terms of measurable quantities,  $C_A$ ,  $C_B$ , or  $C_{AB}$ .

$$r_{B_2^*} = \frac{1}{2}k_1C_B^2 - k_2C_{B_2^*} - k_3C_{B_2^*}C_A + k_4C_B C_{AB}$$

- $C_{B_2^*}$  is very small and  $r_{B_2^*}$  is considered as 0  $\Rightarrow$  PSSH

$$C_{B_2^*} = \frac{\frac{1}{2}k_1C_B^2 + k_4C_B C_{AB}}{k_2 + k_3C_A}$$

$$r_{AB} = \frac{\frac{1}{2}k_1k_3C_B^2C_A - k_2k_4C_B C_{AB}}{k_2 + k_3C_A} \quad (6)$$

- If  $k_2$  is **very small**, equation (6) can be simplified as

$$r_{AB} = \frac{1}{2}k_1C_B^2 \quad \Rightarrow \text{This satisfies the observation given in the statement.}$$

- If  $k_4$  is **very small**, equation (6) can be simplified as

$$r_{AB} = \frac{(k_1k_3/2k_2)C_B^2C_A}{1 + (k_3/k_4)C_A} \quad \Rightarrow \text{If } C_A \text{ is small it can be expressed as } r_{AB} = \frac{k_1k_3}{2k_2}C_B^2$$

2. The acid-catalyzed irreversible liquid phase reaction is carried out adiabatically in a CSTR. The reaction is second order in A. The feed, which is equal molar in water (which contains the catalyst) and A, enters the reactor at a temperature of 47°C and a total volumetric flow rate of 10 dm<sup>3</sup>/min. The concentration of A entering the reactor is 3 mole.

a) What is the reactor **volume** to achieve 80% conversion? (20)

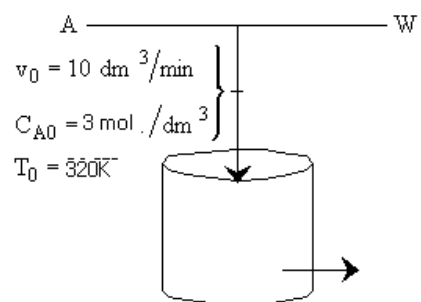
b) What **conversion** can be achieved in a 1000 dm<sup>3</sup> CSTR? What is the exit temperature? (30)

Additional information

$$\Delta H_{Rx} = -3,100 \text{ cal/mol} \quad C_{Pw} = 18 \text{ cal/mol}\cdot^\circ\text{C}$$

$$C_{PA} = 15 \text{ cal/mol}\cdot^\circ\text{C} \quad k = 0.005 \text{ at } 25^\circ\text{C}$$

$$C_{PB} = 15 \text{ cal/mol}\cdot^\circ\text{C} \quad E = 15,000 \text{ cal/mol}$$



(a) Mole Balance

$$V = \frac{F_{A0}X}{-r_A}$$

Energy Balance

$$X_{MB} = \sum \theta_i C_{p,i} (T - T_0) / -\Delta H_{Rx}$$

$$X = \frac{(C_{p,A} + C_{p,W})(T - T_0)}{-\Delta H_{Rx}}$$

$$T - T_0 + \frac{(-\Delta H_{Rx})}{C_{p,A} + C_{p,W}} X$$

$$T = 320 + \frac{3100}{15 + 18} X = 320 + 93.9X$$

For 80% conversion  $T = 320 + (93.9)(0.8) = 395.1 \text{ K}$ 

At 395.1 K

$$k = 0.005 \exp \left[ \frac{15000}{1.987} \left( \frac{1}{298} - \frac{1}{395.1} \right) \right] = (0.005)(505.6) = 2.528 \frac{\text{dm}^3}{\text{mol} \cdot \text{s}}$$

$$V = \frac{1}{k C_{A0}} \left( \frac{X}{(1-X)^2} \right) = \frac{1}{(2.528)(3)} \left( \frac{0.8}{(1-0.8)^2} \right) = 2.64 \text{ dm}^3$$

(b) What conversion can be achieved in a 1000 dm<sup>3</sup> CSTR? What is the exit temperature?

$$-r_A = k C_A^2$$

$$C_A = C_{A0}(1-X) \quad , \quad F_{A0} = C_{A0} v_0 \quad , \quad \tau = \frac{V}{v_0}$$

$$V = \frac{F_{A0}X}{k C_{A0}^2 (1-X)^2} \quad , \quad \tau = \frac{1}{k C_{A0}} \frac{X}{(1-X)^2}$$

$$\tau k C_{A0} = \frac{X}{(1-X)^2}$$

$$\tau k C_{A0} - 2\tau k C_{A0}X + \tau k C_{A0}X^2 - X$$

$$\tau k C_{A0}X^2 - (2\tau k C_{A0} + 1)X + \tau k C_{A0} = 0$$

$$X = \frac{(2\tau k C_{A0} + 1) - \sqrt{(2\tau k C_{A0} + 1)^2 + 4(\tau k C_{A0})^2}}{2\tau k C_{A0}}$$

$$X = \frac{2\tau k C_{A0} + 1 - \sqrt{4(\tau k C_{A0})^2 + 4\tau k C_{A0} + 1 - 4(\tau k C_{A0})^2}}{2\tau k C_{A0}}$$

Let

$$Da = \tau k C_{A0}$$

$$X_{MB} = \frac{(2\tau k C_{A0} + 1) - \sqrt{4\tau k C_{A0} + 1}}{2\tau k C_{A0}} = \frac{(2Da + 1) - \sqrt{4Da + 1}}{2Da}$$

$$X_{MB} = \frac{(2Da + 1) - \sqrt{4Da + 1}}{2Da}$$

where  $Da = \tau k C_{A0} = C_{A0} k_1 e^{\frac{E}{R} \left( \frac{1}{T_1} - \frac{1}{T} \right)}$

$$X_{EB} = T_o + \frac{(-\Delta H_{Rx})T}{(C_{PA} + C_{PW})}$$

$$X_{EB} = (T - 320)/93.9$$

The exit temperature and conversion are determined from the intersection of  $X_{EB}$  and  $X_{MB}$

At **411.6 K**

$$X_{EB} = (411.6 - 320)/93.9 = 0.976$$

$$X_{MB} = 0.976$$

