

4. Applications of the Design Equations for Continuous-Flow Reactor I

- 1st order dependence

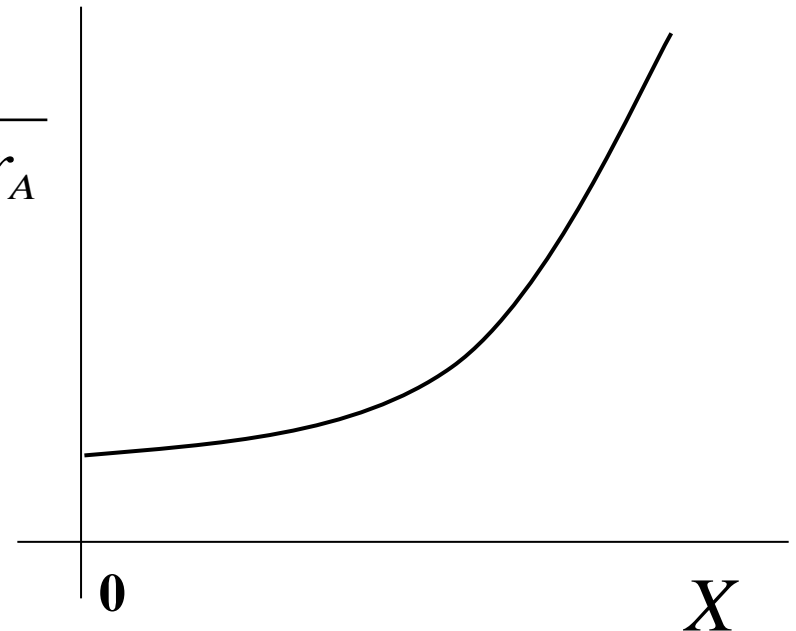
$$-r_A = kC_A = kC_{A0}(1 - X)$$

- k is specific constant, ftn of only Temp.

C_{A0} , entering concentration

- Rearrange

$$\frac{1}{-r_A} = \frac{1}{kC_{A0}} \left(\frac{1}{1 - X} \right)$$



4. Applications of the Design Equations for Continuous-Flow Reactor II

- Reactor size of CSTR and PFR
 - Raw data

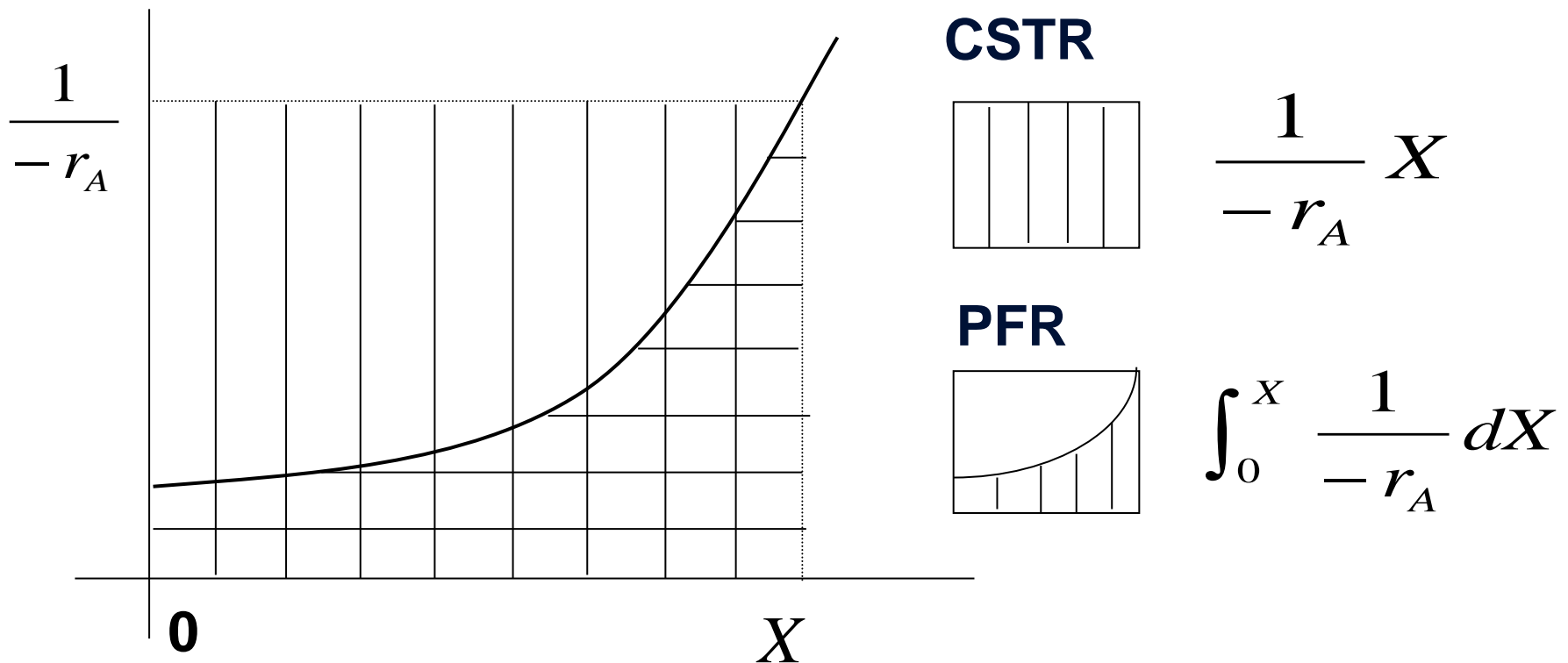
X	0.0	0.1	0.2	0.4	0.6	0.7	0.8
$-r_A$(mol/m³s)	0.45	0.37	0.30	0.195	0.113	0.079	0.05
$(1/-r_A)$(m³s/mol)	2.22	2.70	3.33	5.13	8.85	12.7	20

- Manipulated

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$(1/-r_A)$(m³s/mol)	2.22	2.70	3.33	5.13	8.85	12.7	20
$[F_{A0}/-r_A]$(m³)	0.89	1.08	1.33	2.05	3.54	5.06	8.0

4. Applications of the Design Equations for Continuous-Flow Reactor II

- Reactor sizing



Plots for sizing CSTR and PFR

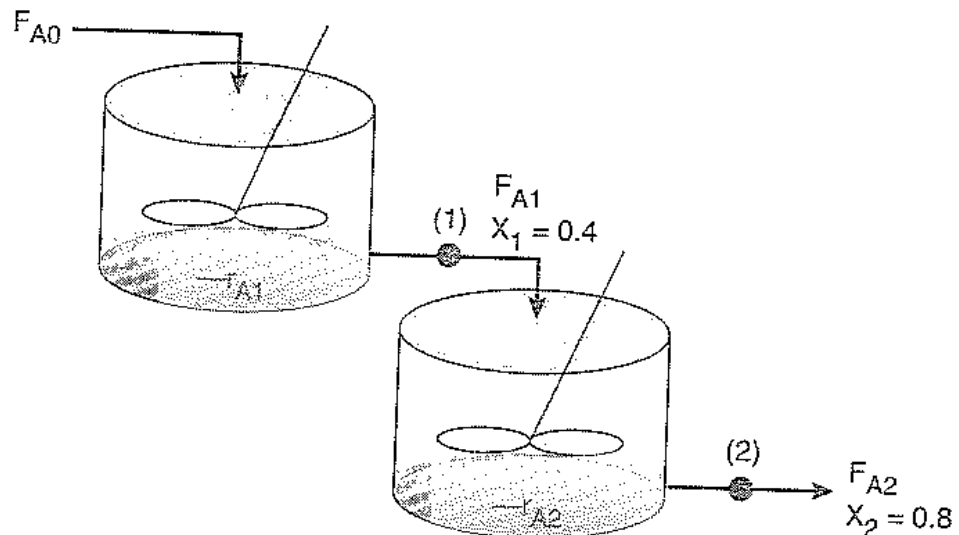
5. Reactors in Series I

- Given $-r_A$ as a function of conversion, one can also design any sequence of reactors

$$X_i = \frac{\text{moles of A reacted up to a point } i}{\text{moles of A fed to first reactor}}$$

Only valid if there are no side streams

- CSTRs in series 1



5. Reactors in Series II

○ CSTRs in series 2

- Reactor 1

$$\text{In} - \text{Out} + \text{Generaton} = 0$$

$$F_{A0} - F_{A1} + r_{A1}V_1 = 0$$

- molar flow rate of A at point 1 is

$$F_{A1} = F_{A0} - F_{A0}X_1$$

$$V_1 = F_{A0} \left(\frac{1}{-r_{A1}} \right) X_1$$

- Reactor 2

$$\text{In} - \text{Out} + \text{Generaton} = 0$$

$$F_{A1} - F_{A2} + r_{A2}V_2 = 0$$

- molar flow rate of A at point 2 is

$$F_{A2} = F_{A0} - F_{A0}X_2$$

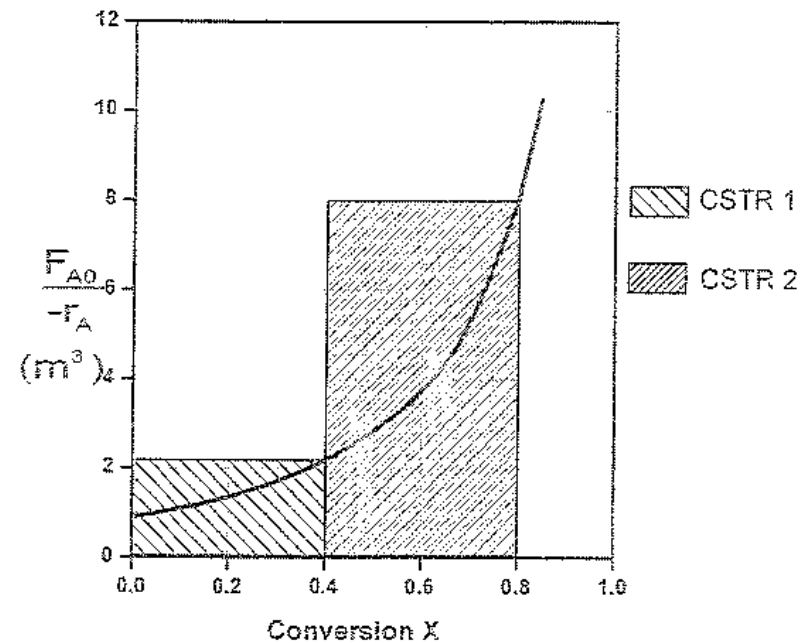
5. Reactors in Series III

○ CSTRs in series 3

- Combining & rearranging

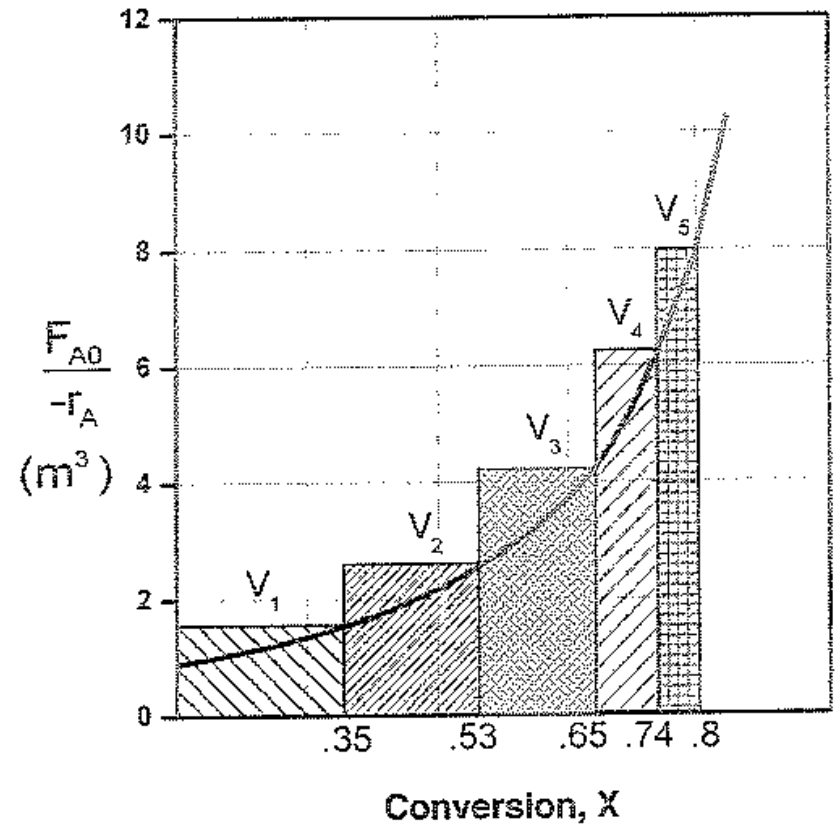
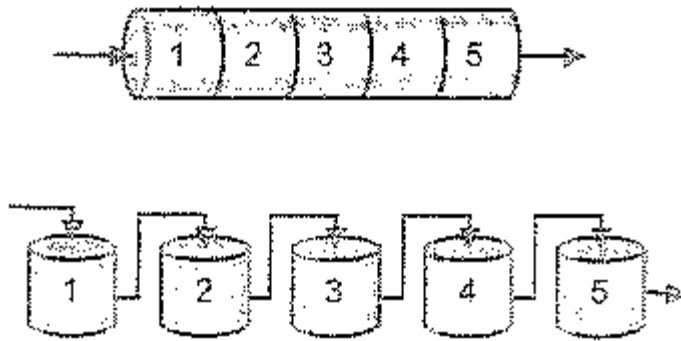
$$V_2 = \frac{F_{A1} - F_{A2}}{-r_{A2}} = \frac{(F_{A0} - F_{A0}X_1) - (F_{A0} - F_{A0}X_2)}{-r_{A2}}$$

$$V_2 = \frac{F_{A0}}{-r_{A2}} (X_2 - X_1)$$



5. Reactors in Series IV

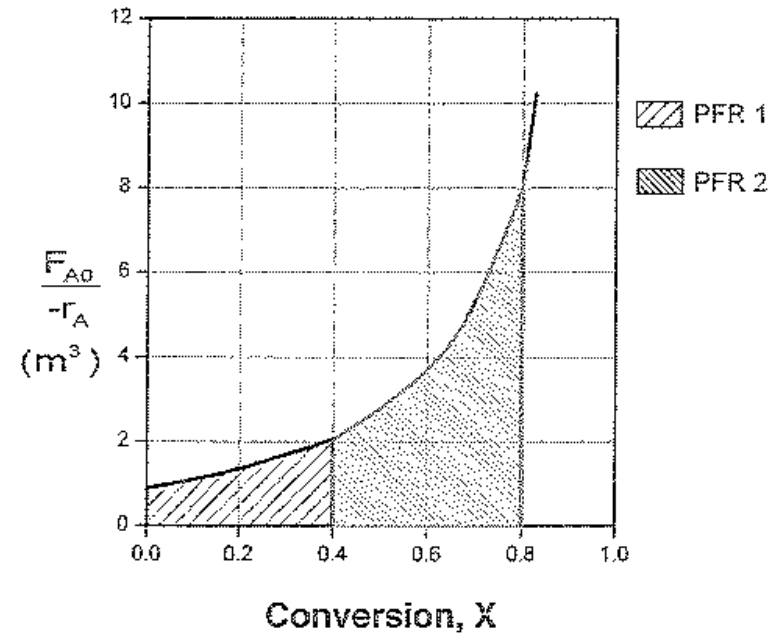
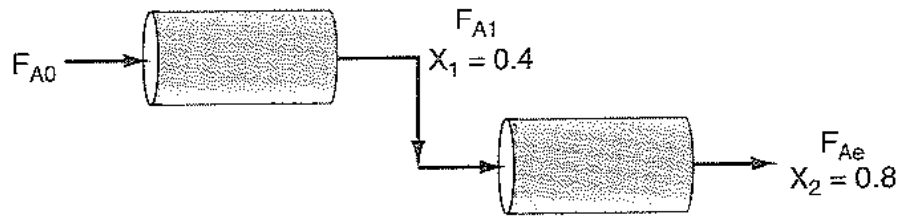
- CSTRs in series 4
 - Large number of CSTRs in series
⇒ PFR approximation



5. Reactors in Series V

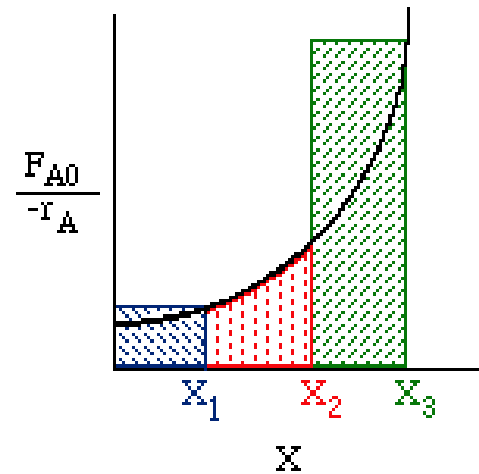
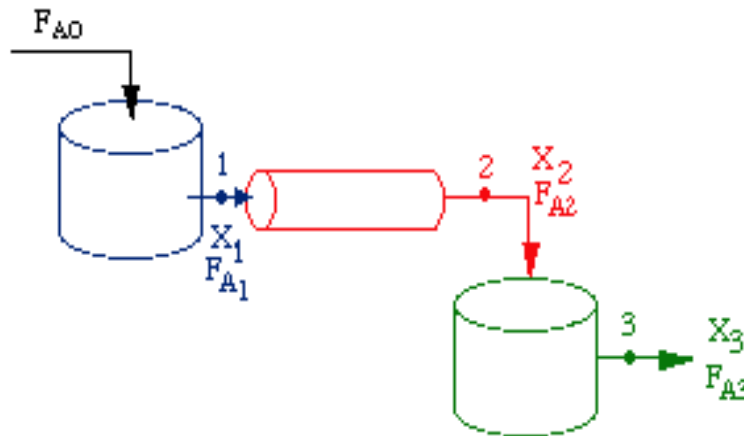
- PFRs in series
 - By definition

$$\int_0^{X_2} F_{A0} \frac{dX}{-r_A} = \int_0^{X_1} F_{A0} \frac{dX}{-r_A} + \int_{X_1}^{X_2} F_{A0} \frac{dX}{-r_A}$$



5. Reactors in Series VI

- Consider a PFR between two CSTRs



$$V_1 = \frac{F_{A0} X_1}{-r_{A1}}$$

$$V_2 = \int_{X_1}^{X_2} \frac{F_{A0}}{-r_{A2}} dX$$

$$V_3 = \frac{F_{A0}(X_3 - X_2)}{-r_{A3}}$$

5. Reactors in Series VII

○ Example 1

- For the irreversible gas-phase reaction: the following correlation was determined from laboratory data (the initial concentration of A is 0.2 g mol/L):

$$\text{For } X \leq 0.5: \frac{10^{-8}}{-r_A} = 3.0 \frac{\text{m}^3 \bullet \text{s}}{\text{mol}}$$

$$\text{For } X > 0.5: \frac{10^{-8}}{-r_A} = 3.0 + 10(X - 0.5) \frac{\text{m}^3 \bullet \text{s}}{\text{mol}}$$

The volumetric flow rate is 5 m³/s.

- Over what range of conversions are the plug-flow reactor and CSTR volumes identical?

5. Reactors in Series VIII

- **Example 1**

- b. What conversion will be achieved in a CSTR that has a volume of 90 L?**

- c. What plug-flow reactor volume is necessary to achieve 70% conversion?**

- d. What CSTR reactor volume is required if effluent from the plug-flow reactor in part (c) is fed to a CSTR to raise the conversion to 90%?**

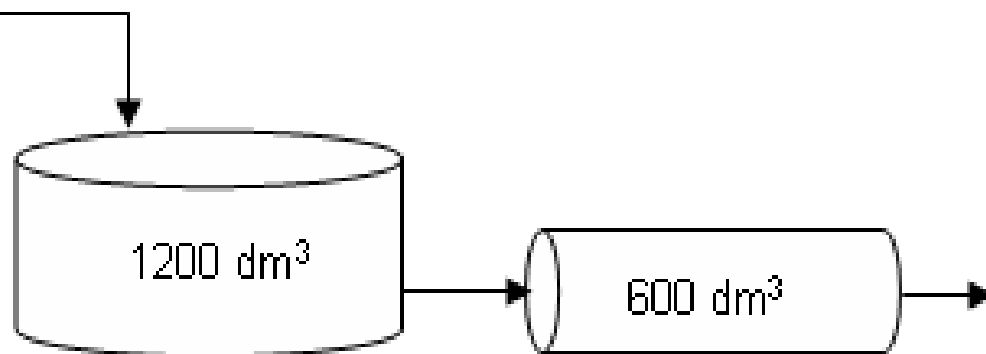
- **Example 2**

5. Reactors in Series IX

○ Example 2

- Pure A is fed at a volumetric flow rate of $1000 \text{ dm}^3/\text{h}$ and at a concentration of 0.005 mol/dm^3 to an existing CSTR, which is connected in series to an existing tubular reactor.

$$C_{A0} = 0.005 \text{ mol/dm}^3$$
$$v_0 = 1000 \text{ dm}^3/\text{s}$$



$$V_{\text{CSTR}} = 1200 \text{ dm}^3, V_{\text{tubular}} = 600 \text{ dm}^3,$$

$X_1, X_2 = ?$ The reciprocal rate vs. conversion given

5. Reactors in Series X

○ Example 2

- The reciprocal rate vs. conversion given

