



# Mass transfer

## Lecture 07: *McCabe-Thiele Method*

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# Learning objectives

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- **Calculate  $q$  and construct the operating line for the given feed condition.**
- **Become capable of constructing operating lines for the continuous fractionation, and calculating the number of ideal plates needed.**
- **Analyze how the reflux ratio affects the number of plates needed, and determine the optimal ratio for a given separation.**

# Today's outline

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- **McCabe-Thiele method**

- ✓ Effect of feed condition
- ✓ Feed line
- ✓ Construction of operating lines, feed plate location
- ✓ Heating and cooling requirements
- ✓ Example 21.2
- ✓ Minimum number of plates & minimum reflux
- ✓ Invariant zone & optimum reflux ratio
- ✓ Example 21.3

# 21.3 Effect of feed condition

- **$q$  represents the fraction of liquid in the feed stream.**

$$q = \frac{\text{heat needed to evaporate 1 mol of feed at entering conditions}}{\text{molar latent heat of vaporization of feed}}$$

$$= \frac{H_V - H_F}{H_V - H_L} = \frac{(H_V - H_L) + (H_L - H_F)}{H_V - H_L} = 1 + \frac{H_L - H_F}{H_V - H_L}$$

$H_V$ : enthalpy at the dew point  
 $H_F$ : enthalpy of feed at the entrance  
 $H_L$ : enthalpy at the boiling point

✓  $q = 1 - f$

- ✓  $q$  can also be calculated as shown in below: **(homework)**

$$q = 1 + \frac{C_{pL}(T_b - T_F)}{\lambda} \quad (\text{cold liquid}) \quad \text{vs.} \quad q = 1 + \frac{C_{pV}(T_F - T_d)}{\lambda} \quad (\text{Superheated vapor})$$

where  $C_{pL}$ ,  $C_{pV}$  represent specific heats of liquid and vapor, respectively;  
 $T_F$ ,  $T_b$ , and  $T_d$  are feed, bubble-point, and dew-point temperature;  $\lambda$  denotes heat of vaporization

# 21.3 Feed line

- Most columns operate w/ the feed as liquid @ ~ b.p.
- $q$  can be used to further analyze the material balance:

- ✓  $L_m = L_n + qF$   
 $V_n = V_m + (1 - q)F$

- ✓ At the feed, two operating lines intersect:

$$V_n y = L_n x + Dx_D$$

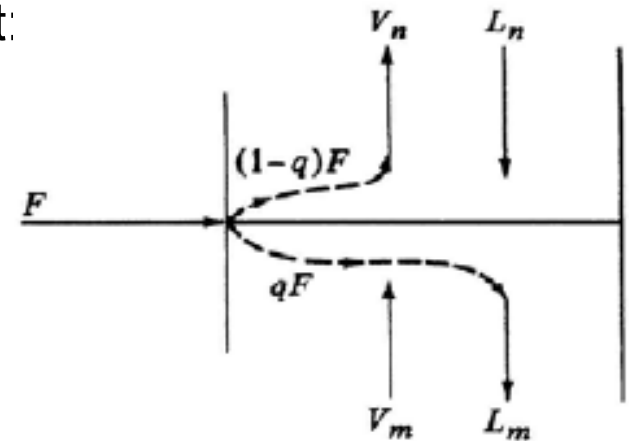
$$V_m y = L_m x - Bx_B$$

- ✓ Subtraction and rearrangement gives:

$$(V_m - V_n)y = (L_m - L_n)x - (Dx_D + Bx_B)$$

$$Fx_F = Dx_D + Bx_B$$

$$y = \frac{q}{q-1}x - \frac{x_F}{q-1}$$



# 21.3 Operating lines

- The simplest method of plotting the operating lines consists of the following 3 steps:

(1) Locate the feed line

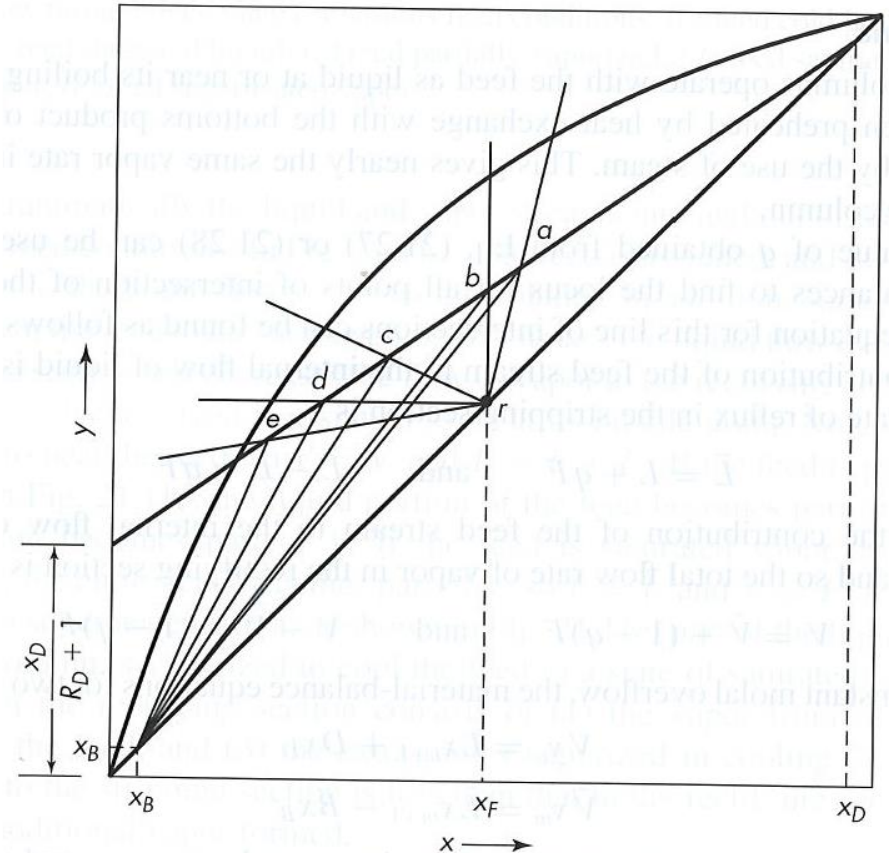
$$y = \frac{q}{q-1}x - \frac{x_F}{q-1}$$

(2) Plot the operating line for the rectifying section

- $x_D/(R_D+1)$
- $(x_D, x_D)$

(3) Plot the operating line for the stripping section

- $x_B, x_B$
- Intersection w/ the rectifying  
@ ???



✓ What about lines a~e?

# 21.3 Feed plate location

- Use the operating lines to calculate the number of ideal plates need.

✓ start from top vs bottom?

- Locate the feed plate such that the number of plates is the smallest:

✓ After the feed plate, you move to the operating line of the different section

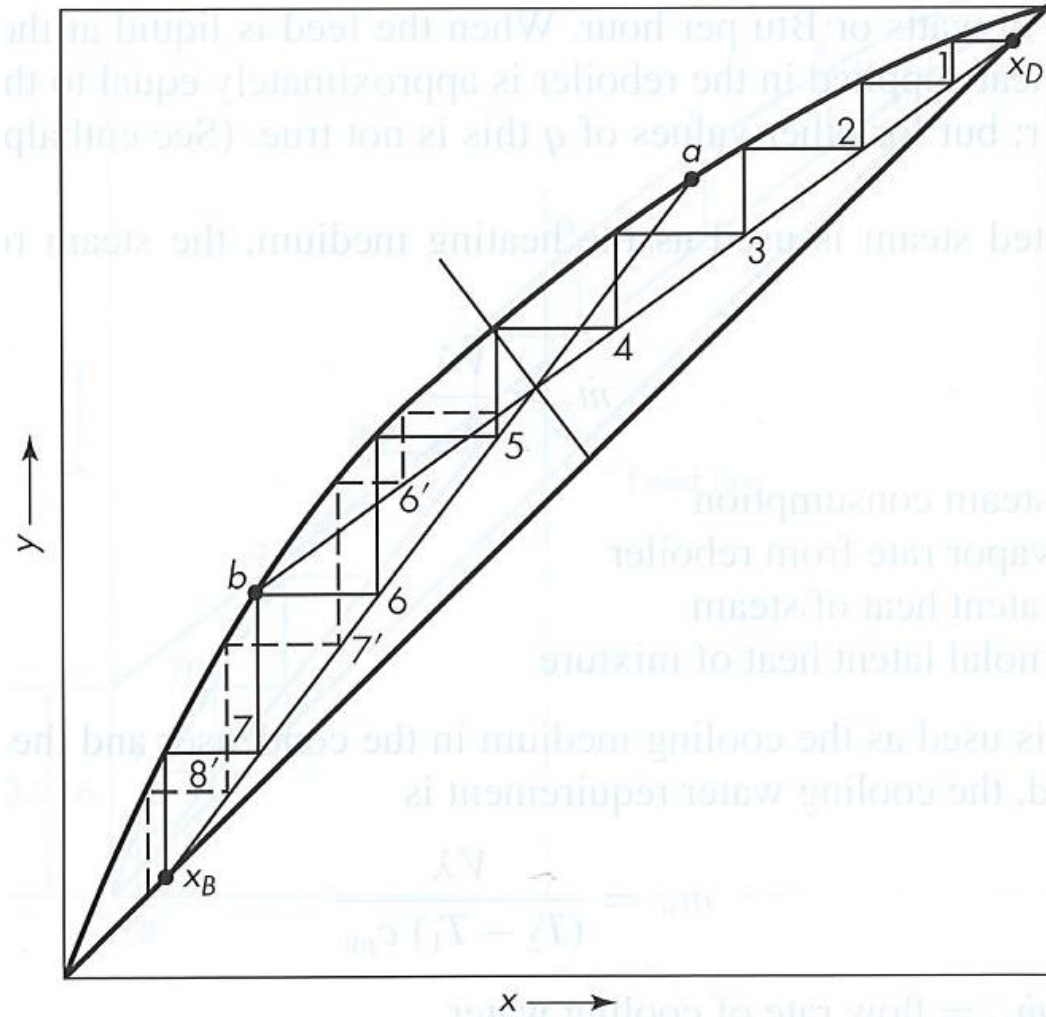


FIGURE 21.13

Optimum feed plate location: —, with feed on plate 5 (optimum location); - - - - -, with feed on plate 7.

# 21.3 Heating & cooling

- **One can consider the column as being adiabatic.**

- ✓ Heat effects are confined to the condenser and reboiler.

- ✓ Heat added to the reboiler ( $q_r$ ) is used to create the vapor flow:

$$q_r = \bar{V} \lambda$$

where  $\bar{V}$  is the vapor rate from the reboiler

- ✓ If the saturated steam is used as the heating medium, the steam required at the reboiler is

$$\dot{m}_s = \frac{\bar{V} \lambda}{\lambda_s}$$

where  $\lambda_s$  is the latent heat of steam

- ✓ If water is used as the cooling medium and the condensate is not subcooled, the water required at the condenser is

$$\dot{m}_w = \frac{V \lambda}{(T_2 - T_1) C_{p,w}}$$

where  $T_2 - T_1$  is the temperature rise of the cooling water



# 21.3 Continuous fractionating

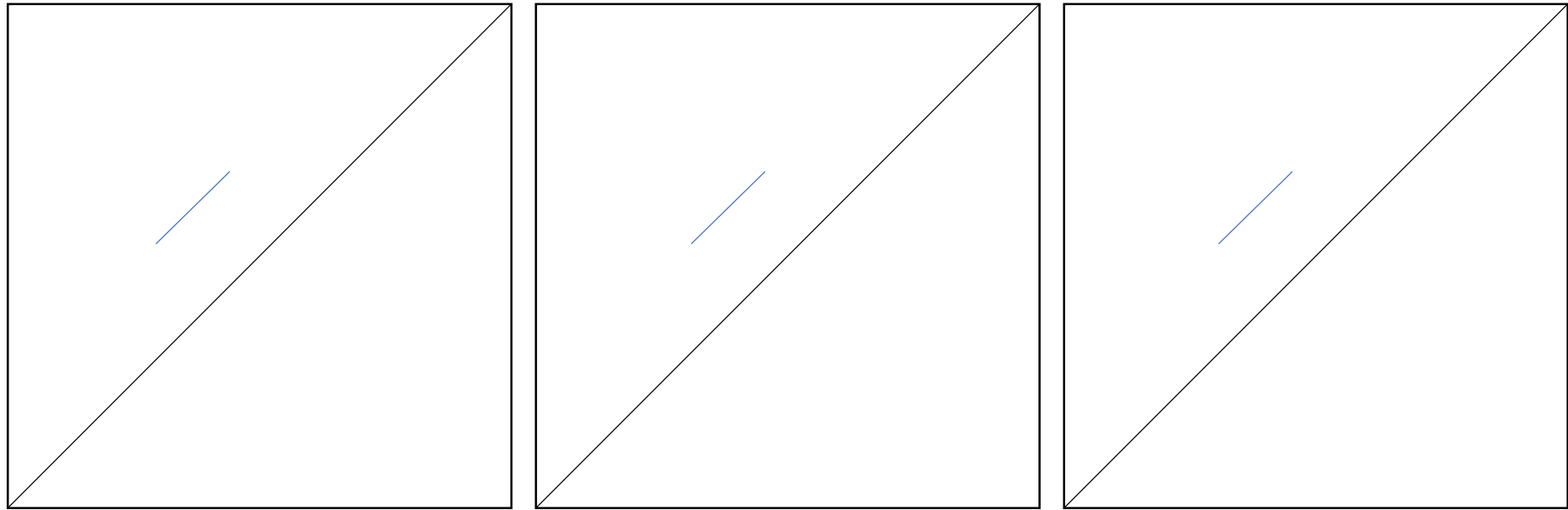
**Ex. 21.2.** A continuous fractionating column is to be designed to separate 30,000 kg/h of a mixture of 40 wt% benzene and 60 wt% toluene into an overheated product containing 97 wt% benzene and a bottom containing 98 wt% toluene. A reflux ratio of 3.5 mol to 1 mol of product is used. The molal latent heats of benzene and toluene are 7,360 and 7,960 cal/mol. Benzene and toluene form a nearly ideal system with relative volatility of about 2.5; the equilibrium curve is shown in below. The feed has a boiling point of 95 °C @ 1 atm. (**In-class & homework**)

- (a) Calculate the moles of overheated product and bottom product per hour.
- (b) Determine the number of ideal plates and the position of the feed for three different conditions of the feed.
- (c) If steam is used for heating, how much steam is required per hour?
- (d) If cooling water enters the condenser at 25 °C and leaves at 40 °C, how much cooling water is required per hour?

Benzene:  $C_6H_6$ , Toluene:  $C_7H_8$

# 21.3 Continuous fractionating

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# 21.3 Minimum number of plates

- The number of plates becomes minimum at **total reflux**:
  - ✓ Why is this the case? (Explain graphically)
  - ✓  $R_D \rightarrow \infty$ , meaning the slope of the rectifying line becomes 1
  - ✓  $F = D = B = 0$ .
  - ✓ The operating line becomes the diagonal line, and no feed line.
  - ✓ For ideal mixtures, a simple method is available for calculating the number of plates needed:

Using relative volatility,  $y = \frac{\alpha x}{1 + (\alpha - 1)x}$  where  $x, y$ , are equilibrium conc.

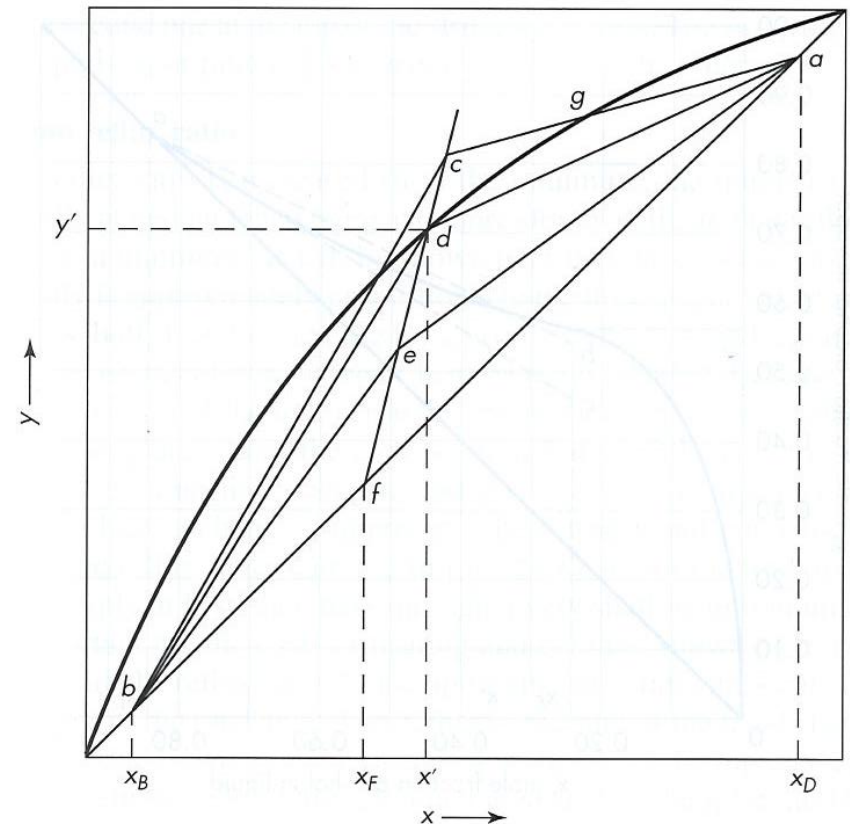
And going through a series of mathematical manipulations,

$$N_{min} = \frac{\ln[x_D(1-x_B)/x_B(1-x_D)]}{\ln \alpha_{AB}} \quad (\text{Fenske equation})$$

if  $\alpha$  changes much, use the geometric mean.

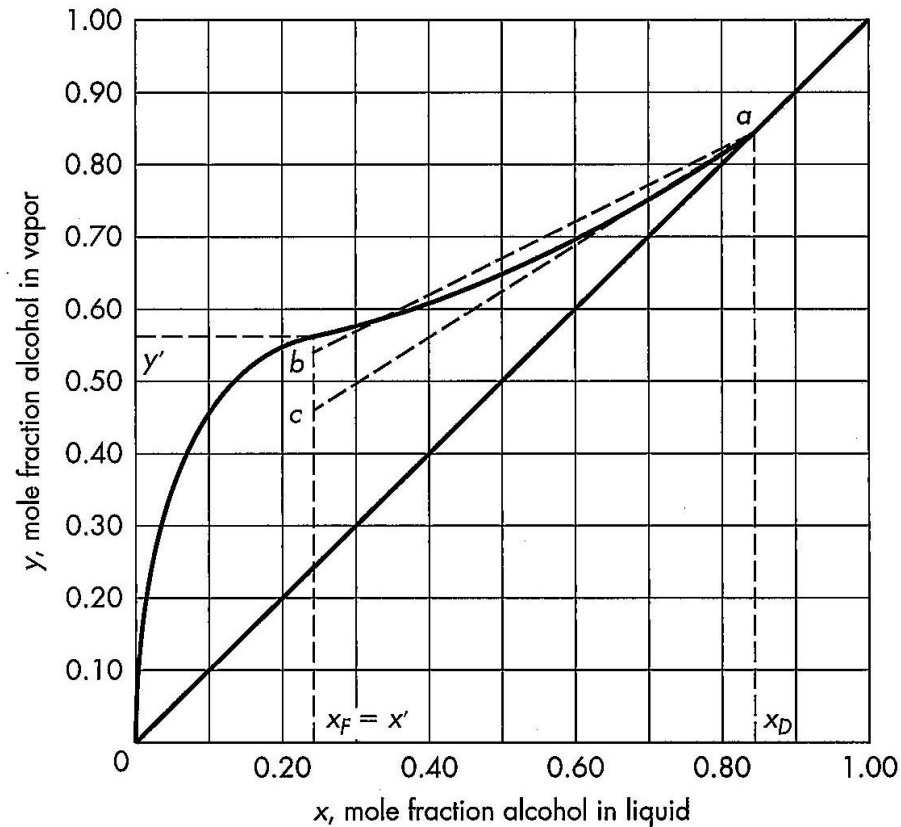
# 21.3 Minimum reflux

- The number of plates becomes infinite at **minimum reflux**:
  - ✓ All actual columns operate at the *intermediate* reflux ratio.
  - ✓ This is when either or both of the operating lines touch the equilibrium curve, meaning infinite steps needed to cross the lines.
  - ✓ If  $R_{Dm}$  is the minimum reflux ratio, the slope of the operating line for the rectifying is  $R_{Dm}/(R_{Dm} + 1)$ , and **it becomes ???**



# 21.3 Minimum reflux

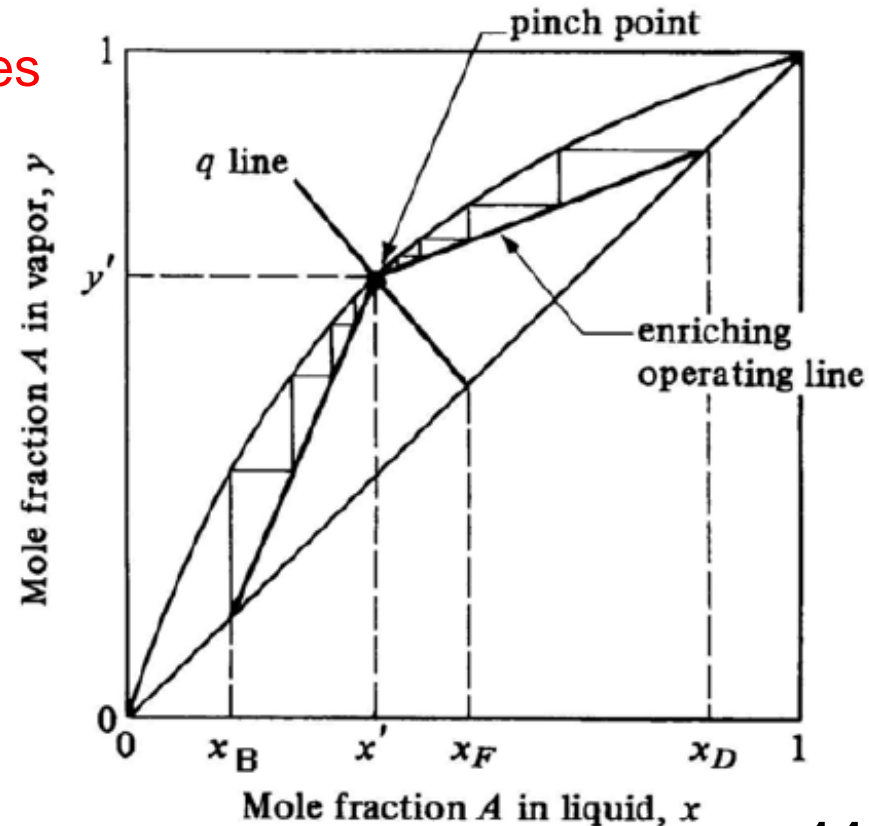
- The previous eqn. is not always true. For example,



**FIGURE 21.18**  
Equilibrium diagram (system ethanol-water).

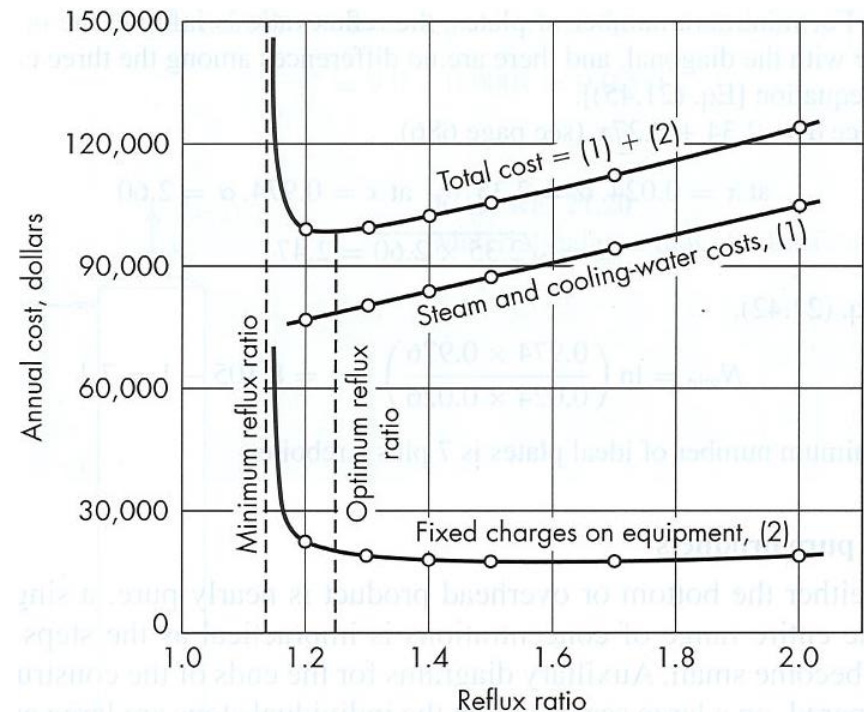
# 21.3 Invariant zone

- There can exist an infinite number of ideal plates in which no changes occur w.r.t. liquid/vapor concentration.
  - ✓  $x_{n+1} = x_n$  and  $y_{n-1} = y_n$
  - ✓ The term *pinch point* is also used.
  - ✓ Where (top? Bottom? Middle?) does the zone form when the min. reflux ratio is used?



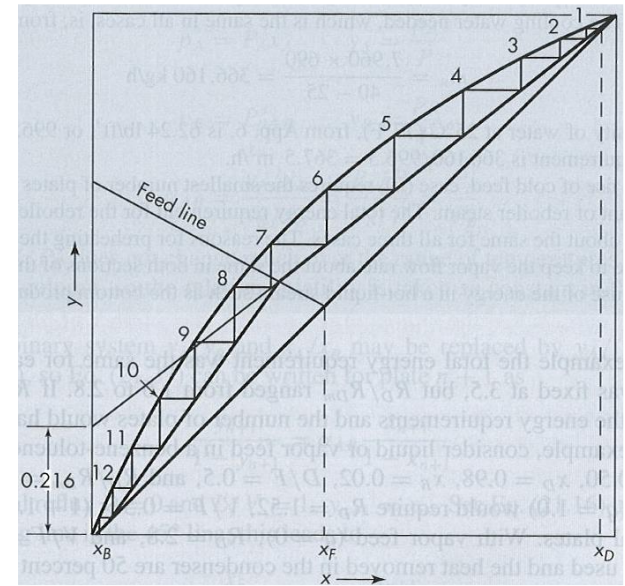
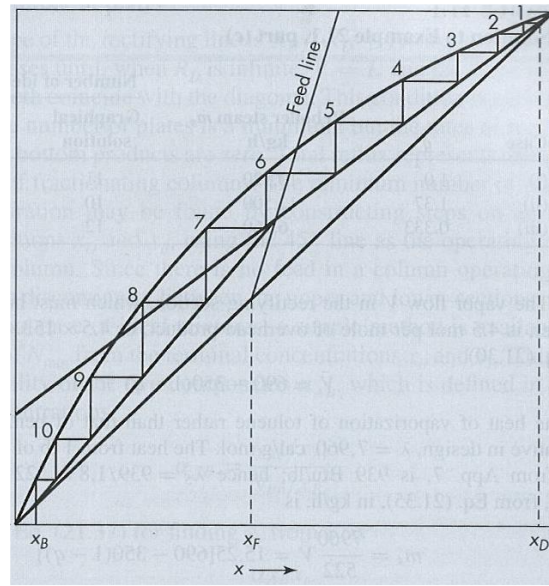
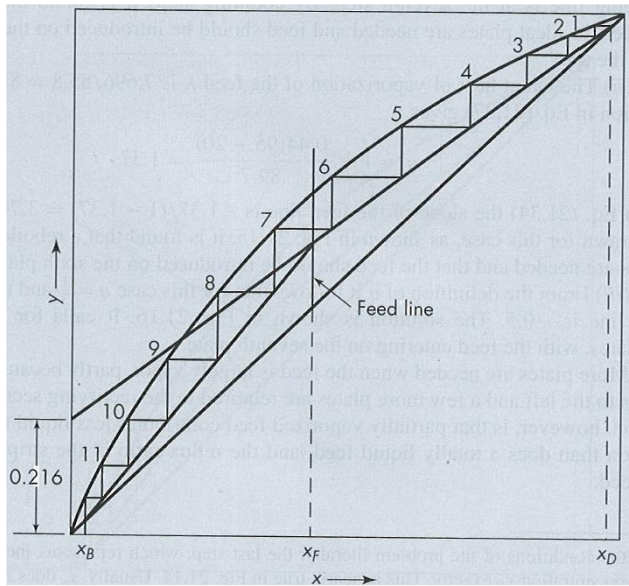
# 21.3 Optimum reflux ratio

- Cross-sectional area of the column is often proportional to the vapor flow rate.
- As reflux ratio increases,  $V$  &  $L$   $\uparrow$  as well as column diameter; number of plates needed **increase/decrease?**
  - ✓ Total cost is proportional to #plates x cross-sectional area
  - ✓ **Optimal reflux ratio is the one resulting in the min total cost!**



# 21.3 Minimum ratio and plates

Ex. 21.3. What are (a) the minimum reflux ratio and (b) the minimum number of plates for cases (b)(i), (b)(ii), and (b)(iii) of Ex. 21.2? (**In-class**)



$$q = 0.33, 1, 1.37$$