Cesium Carbonate에 의한 이산화탄소의 흡착 해석

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Sorption Analysis of Carbon Dioxide onto Cesium Carbonate

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INTRODUCTION

In mass transfer processes that accompany chemical reactions, the diffusion may have an effect on the reaction kinetics. The simplest and the most commonly used models for non-catalytic heterogeneous gas-solid reactions are the shrinking-core model and the homogeneous model with negligible pore diffusion limitations. Also, the deactivation model has been used to obtain the reaction kinetics using an analysis of reactivity of the solid reactant, which may be decreased by the changing the reaction circumstances. We believe that it is worthwhile to investigate the reaction kinetics of gas-solid heterogeneous reaction, such as the $CO₂$ -carbonate reaction, from a comparison among these models.

In our previous work (1), we studied the sorption kinetics of the gas-solid reaction between $CO₂$, H₂O, and Na₂CO₃ using breakthrough data of CO₂ in series. In this study, Cs₂CO₃ was used as a sorbent of $CO₂$ to analyze the sorption kinetic using breakthrough data of $CO₂$ in a fixed bed, comparing the shrinking-core model, the homogeneous model and the deactivation model even though the carbonation mechanism of Rb_2CO_3 by CO_2 and moisture is very complicated.

THEORY

The formation of a dense product layer over the solid reactant creates an additional diffusion resistance and is expected to cause a drop in the reaction rate. One would also expect it to cause significant changes in the pore structure, active surface area, and activity per unit area of solid reactant with respect to the extent of the reaction. All of these changes cause a decrease of activity of the solid reactant with time. In the deactivation model, the effects of all of these factors on the diminishing rate of CO₂ capture were combined in a deactivation rate term.

With assumptions of a pseudo-steady state and a constant concentration of water vapor, the isothermal species conservation equation for the reactant gas $CO₂$ in the fixed bed is

$$
-Q_g \frac{dC_A}{dw} - k_o C_A \alpha = 0
$$
 (1)

where $k_0 = kC_w$, α and Q_g are reaction activity of absorbent and volumetric flow rate of gaseous mixture, respectively.

In writing this equation, axial dispersion in the fixed bed and any mass transfer resistances were assumed to be negligible. According to the proposed deactivation model, the rate of change of α is expressed as

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$$
-\frac{d\alpha}{dt} = k_d C_A^{\ n} \alpha^m
$$
 (2)

where k_d is the deactivation rate constant. The zeroth solution of the deactivation models is obtained by taking n=0. m=1, and the initial activity of the solid as unity.

$$
a = \exp[-\frac{k_0 w}{Q_g} \exp(-k_d t)]
$$
\n(3)

This solution is equivalent to the breakthrough equation proposed by Suyadal and coworkers [2] and assumes a fluid phase concentration that is independent of deactivation processes along the reactor. More realistically, one would expect the deactivation rate to be concentration-dependent and, accordingly, axial-position-dependent in the fixed bed.

To obtain the analytical solution of Eq. (1) and (2) by taking n=m=1, an iterative procedure was applied. The procedure used here is similar to the procedure proposed by Dogu [3] for the approximate solution of nonlinear equations. In this procedure, the zeroth solution [Eq.(3)] is substituted into Eq. (2), and the first correction for the activity is obtained by the integration of this equation. Then, the corrected activity expression is substituted into Eq. (1), and integration of this equation gives the first corrected solution for the breakthrough curve.

$$
a = \exp\left[\frac{\left[1 - \exp\left(\frac{k_{o}w_{f}}{Q_{g}}(1 - \exp(-k_{d}t))\right)\right]}{1 - \exp(-k_{d}t)}\right] \exp(-k_{d}t)
$$
\n(4)

This iterative procedure can be repeated for further improvement of the solution. In this procedure, higher-order terms in the series solutions of the integrals are neglected. The breakthrough curve for the deactivation model with two parameters (k_0 and k_d) is calculated from the concentration profiles by Eq. (4).

EXPERIMENTAL

Sorption experiments were carried out in the presence of carbon dioxide and moisture with cesium carbonate sorbent in a fixed bed pyrex glass reactor. Water vapor was fed to the reactor through a line heated using a micro syringe. The flow rates of gas mixture of carbon dioxide and nitrogen were within the range of 6-20 cm³/min (measured at 25° C); the composition of CO₂ in the gas mixture was 12 % in most of the experiments. The flow rate of water was in the range 0.6-3 cm³/h. The amount of sorbent was in the range 0.5-2 g. Experiments were repeated over a temperature range between 50 and 80°C. A gas chromatograph (detector: thermal conductivity detector; column: Haysep D (10 feet by 1/8 inch of stainless steel); detector temperature: 190°C; feed temperature: 160°C; flow rate of He: 25.7 cm³/min; retention times of N₂, CO₂, and H₂O: 0.9, 1.323, 20.6 min, respectively) connected to the exit stream of the reactor allowed for on-line analysis of $CO₂$, $N₂$, and water. The experimental procedure used to obtain the breakthrough data of $CO₂$ duplicated in detail the reported approach [1].

RESULTS AND DISCUSSION

The measured values of breakthrough curves of $CO₂$ were plotted against the reaction time, with

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parameters of the flow rate of the gaseous mixtures of $CO₂$ and N₂ and water indicated as various symbols in Fig. 1. As shown in Fig. 1, a shift of the breakthrough curves to shorter times was observed at greater flow rate of the gaseous mixture with a decrease in sorption capacity. This result means that the reaction conversion decreases as the space time of the gaseous mixtures in the fixed bed, i.e., the reaction time, decreases. Analysis of the experimental breakthrough data using a nonlinear least-squares technique gave a very good agreement with Eq. (4). The calculated curves using Eq. (4) are shown in Fig. 1 as solid lines with regression coefficient greater than 0.996.

Fig. 1. Effect of the flow rate of mixture of N_2 and CO_2 on the breakthrough curve of CO_2 at 60^oC and $W_0 = 1.5$ g.

To obtain the dependence of reaction parameters on the sorption temperature (T), the breakthrough curves of $CO₂$ were measured in the temperature range between 50 and 80 $^{\circ}$ C at flow rate and concentration of CO_2 in gaseous mixture of CO_2 and N_2 of 10 cm³/min and 0.12 mole fraction, respectively, a flow rate of water of 2.98 cm³/h, 1.5 g of sorbent. The values of k_0 and k_d were evaluated from the analysis of the experimental breakthrough data using a nonlinear least-squares technique using the same procedure mentioned above; k was obtained using k_0 and the initial concentration of moisture. The Arrhenius plots are shown in Fig. 7 and 8, respectively. As shown in Fig. 7 and 8, the plots satisfy linear relationship. Using the values of the slopes and intercepts of these straight lines of the Arrhenius plots, the following empirical equations were obtained.

$$
k = 2.184x10^{5} \exp(-\frac{0.159}{RT})
$$
 (5)

$$
k_{d} = 1.189x10^{10} \exp(-\frac{0.682}{RT})
$$
 (6)

CONCLUSIONS

The breakthrough data of CO_2 were measured in a fixed bed to observe the reaction kinetics of CO_2 sorption among cesium carbonate, carbon dioxide, and moisture under the experimental conditions of a flow rate of the gaseous mixture of 6-20 cm³/min, a flow rate of water of 0.6 -3 cm³/h, a potassium

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carbonate mass of 0.5-2 g, and a reaction temperature of $50-80^{\circ}$ C. A good agreement of the deactivation model was obtained with the experimental breakthrough data in the heterogeneous solid-gas reaction system, with respect to changes in the pore structure and the reactivity of the solid reactant. The sorption rate constant and the deactivation rate constant were evaluated through analysis of the experimental breakthrough data using a nonlinear least squares technique and were described in the Arrhenius form.

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